



**BURNSIDE**

**Landfill Expansion Noise Impact  
Assessment**

**St. Marys Future Solid Waste Disposal  
Needs Environmental Assessment**

**Town of St. Marys**

DRAFT

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**April 7, 2016  
300032339.0000**



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## Record of Revisions

Revision	Date	Description
0	April 2016	Initial Submission by Burnside to Town of St. Marys

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## Executive Summary

The Town of St. Marys is conducting an Individual Environmental Assessment under the *Environmental Assessment Act* to review alternative means to manage solid waste disposal in the Town over a forty year planning period. The existing St. Marys landfill site (the "Site"), Environmental Compliance Approval (ECA) Number A150203, is located at 1221 Water St. South, St. Marys, Ontario. The 37 ha Site was part of a former clay borrow pit that was used by St. Marys Cement in cement manufacturing and contains an approved fill area of 8 ha. The landfill is nearing its approved fill capacity and a new means to manage disposal of post-diversion solid waste is required.

All of the sound level limits at all Points of Reception (PORs) for each Alternative Method are below the Ministry criteria; therefore all methods are acceptable potential expansion options for the St. Marys landfill.

Vibration is typically not felt further than 75 m from the source. The closest sensitive receptor is located 148.5 m from the landfill operations so vibration from delivery, placement, compaction and covering the waste within the expanded landfill was considered negligible.

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## 1.0 Project Description

### 1.1 Introduction

The Town of St. Marys is conducting an Individual Environmental Assessment under the *Environmental Assessment Act* to review alternative means to manage solid waste disposal in the Town over a forty year planning period. The existing St. Marys landfill site (the "Site"), Environmental Compliance Approval (ECA) Number A150203, is located at 1221 Water St. South, St. Marys, Ontario. The 37 ha Site was part of a former clay borrow pit that was used by St. Marys Cement in cement manufacturing and contains an approved fill area of 8 ha. The landfill is nearing its approved fill capacity and a new means to manage disposal of post-diversion solid waste is required. The location of the existing landfill is illustrated on Figure 1.

Terms of Reference (TOR) were prepared and were approved by the Ministry of Environment and Climate Change on December 29, 2014. The TOR laid out a strategy for completing the EA. Phase 1 of the EA Methodology evaluated *Alternatives to the Undertaking*, specifically, undertaking a qualitative screening of:

- Alternative 4: exporting waste to another jurisdiction, and
- Alternative 6: expanding the existing landfill.

Phase 1, now completed and documented elsewhere, determined that expanding the existing landfill was preferred. This Landfill Expansion Noise Impact Assessment report therefore looks at the *Alternative Methods* for expanding the St. Marys landfill. The *Alternative Methods* are listed in the table below.

Table 1.1 Alternative Methods

Alternative Methods	Description
1 Vertical expansion of the existing landfill	This <i>Method</i> involves an expansion in the vertical direction within the existing footprint of the landfill.
2 Horizontal expansion of the existing landfill	This involves an expansion outside of the existing landfill footprint.
3 A combination of vertical and horizontal expansion	This <i>Method</i> would involve partial vertical expansion along with some horizontal expansion of the landfill footprint, basically a mixture of <i>Methods</i> 1 and 2.
4 Development of a new landfill footprint	This <i>Method</i> involves closure of the existing 8 ha footprint and development of a new landfill footprint elsewhere on the 37 ha Site.
5 Vertical expansion plus a new footprint	This <i>Method</i> is a combination of <i>Methods</i> 1 and 4.

Each of the *Alternative Methods* are compared against existing conditions and regulatory requirements in this report.

The Current situation and five Alternative Methods of landfill expansion are assessed in this report. For each, the worst case impact was selected for investigation. This choice means that there are substantial periods of time when the activity will be substantially less than modelled and/or that activity will be further from the receptors than modelled so the impacts will be less than predicted.

The Current situation and Alternative Method 1 have the same worst case scenario so the modelling and results indicated as “Current” are the same as “Alternative Method 1”.

Similarly, “Alternative Method 5” has the same worst case scenario as “Alternative Method 3” and so was not modelled separately.

## **1.2 Area of Study**

The identified Study Area will be used as the basis for defining and characterizing the natural environment which may be affected by the expansion.

The Study Areas for this Landfill Expansion Noise Impact Assessment report are defined as follows:

- All lands associated with the existing St. Marys landfill, the 37 ha site located at 1221 Water St. South, St. Mary's, ON.
- All lands 500 m from the noise sources unless modelling indicates impacts exceeding criteria beyond that distance in which case the area will be expanded to show all impacts exceeding criteria.
- Study Area Vicinity- all lands within a 1,000 m radius of the on-site Study Area. Since all sources are expected to be ground level, the significant impacts will all be close to the property line so the EA is only expected to discuss impacts on sensitive receptors within 1 km. Should modelling show impacts outside the 1 km radius, they will be discussed appropriately.

## **1.3 Study Overview**

The approach to this assessment was to satisfy the requirements of the Ontario Environmental Assessment Act (R.S.O. 1990, c. E, October 25, 2010). The Site will be submitting an Environmental Compliance Approval in the future, and as such, this assessment was also done to meet the criteria of the Environmental Protection Act (R.S.O. 1990, c. E, February 1, 2016). This noise and vibration impact assessment is being conducted in support of this process and hence has been prepared based on Ontario Ministry of the Environment and Climate Change (MOECC) requirements.



The landfill currently operates Tuesday, Wednesday, Friday and Saturday between the hours of 8:00 a.m. and 4:30 p.m. Most of the noise generating activities at the Site, including receiving of waste trucks occurs between those hours. The Site ECA allows for operations between 7:00 a.m. and 7:00 p.m., therefore, this assessment is for daytime (7 a.m. to 7 p.m.) noise impact only.

The noise impact considerations for the landfill site, including sound level limits and the potential noise sources considered in the assessment are in accordance with the Ministry publication "Noise Guidelines for Landfill Sites"<sup>1</sup>.

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<sup>1</sup> Noise Guidelines for Landfill Sites (DRAFT). October 1998. Ontario Ministry of the Environment

## **2.0 Noise Assessment**

The noise impact assessment completed for the proposed expansion consists of:

1. Identification of all dominant noise sources at the Site;
2. Determination of worst-case noise emission scenarios associated with the above-mentioned alternative methods;
3. Acoustic modelling of the Site under the defined worst-case operating scenario in order to predict worst-case noise impact at all of the nearby receptor locations;
4. Comparison of the predicted maximum receptor sound levels with the applicable criterion for landfills to determine compliance;
5. Determine noise mitigation measures in case of non-compliance for various options; and
6. Comparison of the various options to assess relative impacts of each option at the sensitive receptors.

### **2.1 Applicable Criteria**

#### **2.1.1 MOECC Noise Limits**

The Ministry's publication Noise Guideline for Landfills – DRAFT (MOE, 1998) applies to the operations at the St. Marys Landfill. The guidelines specified a daytime (7:00 – 19:00) receptor noise criterion of 55 dBA and a nighttime (19:00 – 7:00) receptor noise criterion of 45 dBA. These sound exposure limits apply to any receptor, in any worst-case hour of operation at the landfill. These limits can be replaced with existing background values if it is established that the background levels are consistently higher due to other noise sources in the area, such as road traffic and/or other industries.

### **2.2 Sensitive Receptors**

Receptors of interest for this assessment are consistent with MOE document NPC-300 (MOE, 2013) and include the following noise sensitive land uses:

- Residences;
- Hotels, motels and campgrounds;
- Schools, universities, libraries and daycare centers;
- Hospitals and clinics, nursing / retirement homes; and
- Churches and places of worship.

Receptors of interest within the Study Area are residential houses located along Perth Road 123 and Water Street South. Residences have different setback distances and various degrees of visual screening from the road. Residences closest to the road are anticipated to have the greatest potential impact from the traffic and operation of the landfill. As the separation distance increases between the road and receptors, the impact from sound related to traffic and landfill operation will be reduced.

For the modelling portion of this assessment, points of reception (POR) are chosen to be representative of the receptors of interest with the highest impacts from the Site. The PORs that are representative of worst-case potential noise impacts have been identified and used in the analysis. Receptors are placed in the plane of a window where sound originating from the Site is received, assumed to be at a height of 1.5 m and 4.5 m unless otherwise stated. Six residential locations have been identified as being the most impact sensitive points of reception along Water St. South (Hwy 123). Sound levels at all other receptors will be at or below the sound levels of the representative receptors next to them. The PORs are shown in Figure 3 and summarized in Table 2.

## **2.3 Evaluation of Noise Sources**

St. Marys Landfill contains several significant sources of noise. These sources include on-site traffic and a compactor. All noise sources associated with road traffic travelling to/from St. Marys landfill, as well as all traffic in the Study Area have been included in this assessment. Passenger vehicles<sup>2</sup> are generally considered to have negligible noise emissions when travelling at 20 km/h or less. All vehicles are restricted to 20 km/h while on Site so any noise associated with passenger vehicles has been excluded.

See Table 1: Noise Source Summary Table for a complete list of sources, sound power, source location, existing noise control measures, and required noise control measures.

### **2.3.1 Off-Site Road Traffic**

The 2012 estimate of Annual Average Daily Traffic (AADT) for Perth Road 123 and Water Street South was obtained from Perth County. It has been assumed that the waste quantity will increase 1 % annually, thus it has been assumed that traffic generated to and from the site will increase at a rate of 1 % annually. The current and future AADT estimates are included in Appendix B. Noise at the sensitive receptors was calculated using STAMSON. The model outputs are included in Appendix C.

### **2.3.2 On-Site Traffic**

It is likely that only one or two trucks per hour will be entering the Site. All trucks entering the site will follow OnSiteTrk1 truck path. Once on Site, the trucks will only follow one of OnSiteTrk2, OnSiteTrk3, or OnSiteTrk4 truck paths.

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<sup>2</sup> Passenger vehicles include cars, mini-vans, SUV's and pick-up trucks. See the definition of Automobiles provided in Section 2.4.1.

Eight trucks per day are expected to enter the site following truck path OnSiteTrk1, with a maximum of 4 trucks following OnSiteTrk2, a maximum of 4 trucks following OnSiteTrk3, and a maximum of 2 trucks following OnSiteTrk4. The noise model assumes that in one hour, the maximum number of trucks per day will travel each of the truck paths. Therefore, the noise model is very conservative.

#### **2.3.2.1 OnSiteTrk1**

The moving source labelled OnSiteTrk1 shown in Figure 3 represents the truck traffic entering the Site and driving to the weigh scale, and driving from weigh scale and exiting the Site. It is expected that a maximum of 8 trucks per day will enter the Site. They are all assumed to travel this path in the same hour.

The source emission was estimated from previous measurements taken at another site, and are shown in Table C1 next to the "Delivery Truck Medium Speed" label.

#### **2.3.2.2 OnSiteTrk2**

The moving source labelled OnSiteTrk2 shown in Figure 3 represents the truck traffic driving from the weigh scale to the open face, and returning to the weigh scale. It is expected that a maximum of 4 trucks per day will travel along this truck path. They are all assumed to travel this path in the same hour.

#### **2.3.2.3 OnSiteTrk3**

The moving source labelled OnSiteTrk3 shown in Figure 3 represents the truck traffic driving from the weigh scale to the composting area, and returning to the weigh scale. It is expected that a maximum of 4 trucks per day will travel along this truck path. They are all assumed to travel this path in the same hour.

#### **2.3.2.4 OnSiteTrk4**

The moving source labelled OnSiteTrk4 shown in Figure 3 represents the truck traffic driving from the weigh scale to the stock pile and returning to the weigh scale. It is expected that a maximum of 2 trucks per day will travel along this truck path.

### **2.3.3 On Site Equipment**

While the air emission indicates that the compactor doesn't run more than 20 minutes of any one hour, the noise model assumes that the compactor runs for the entire hour so the noise model is very conservative.

#### **2.3.3.1 Loader (LDR)**

The Loader (LDR) used on site is a 2013 CAT 938K Loader. It was confirmed by on-site employees that the noise from this equipment is minimal. They indicate that while

standing in the garage next to the machine, “It is difficult to tell that it is running” while it is idling. This source has been considered to have negligible noise emissions.

### **2.3.3.2 Compactor (CMPTR)**

The Compactor (CMPTR) used on site is a 1986 CAT 816D Compactor. The source is 2.8 m above the ground. The sound power levels for the loader were established through On-Site measurements on Wednesday March 16, 2016. The sound power levels are in Appendix D. See Appendix E for a photograph.

## **2.4 Modelling Methodology**

Only the Current and three Alternative Methods were modelled because the worst case from the selected Alternative Methods covers all five Alternative Methods discussed in Section 1.1. The Current situation and five Alternative Methods of landfill expansion are assessed in this report. In each case, the worst case impact was selected for investigation. The choice means that there are substantial periods of time when the activity will be substantially less than modelled and/or that activity will be further from the receptors than modelled so the impacts will be less than predicted.

The Current situation and Alternative Method 1 have the same worst case scenario so the modelling and results indicated as “Current” are the same as “Alternative Method 1”.

Similarly, “Alternative Method 4” has the same worst case scenario as “Alternative Method 5” and so was not modelled separately.

### **2.4.1 Off-Site Traffic Noise**

The MOECC requires the use of the ORNAMENT noise model for predicting roadway traffic noise levels as  $LEQ$  (16-hr) Day and  $LEQ$  (8-hr) Night values. The MOECC developed the STAMSON computer program to implement the ORNAMENT methodology in 1990. The methodology detailed within the MOECC NPC-300 guideline was followed for the roadway traffic modelling.

The Study Area was modelled for the existing conditions, as well as for the future noise levels for three landfill expansion scenarios. The road traffic data was projected to year 2025, using a 1 % annual growth rate. In order to predict sound levels from road traffic STAMSON requires:

- Source to receiver distance – between 15 m and 500 m;
- Minimum traffic volume – 40 vehicles per hour;
- Minimum vehicle speed – 80 km/h (as posted on Perth Road 123);

Definitions of vehicle classes used in the model are as follows<sup>3</sup>:

- Automobiles: All vehicles having two axles and four wheels designed primarily for the transportation of nine or fewer passengers or the transportation of cargo (e.g., vans and light trucks). Generally, the gross vehicle weight is less than 4,500 kg.
- Medium Trucks: All vehicles having two axles and six wheels designed for the transportation of cargo. Generally, the gross vehicle weight is greater than 4,500 kg but less than 12,000 kg. Public works vehicles fall into this category, though few dedicated waste collection vehicles are Medium Trucks.
- Heavy Trucks: All vehicles having three or more axles and designed for the transportation of cargo. Generally, the gross vehicle weight is greater than 12,000 kg. Most waste collection vehicles – front, side or rear loaded trucks and roll-off bin trucks – fall into this category.

A number of assumptions were used in the noise model:

- The road gradient was assumed to be 0%.
- Flat/gentle slope topography was selected.
- Road pavement was assumed as a standard asphalt surface.
- Intermediate surface was assumed to be absorptive (grass).
- A minimum 15 m separation distance was assumed to the POR when the actual separation distance was less than 15 m.

Note that the result of this modelling indicates that the road traffic impact is not higher than the exclusionary limit and so the exclusionary limit of 55 dBA during the day is used as the criterion that the landfill operations must meet.

The speed limit is reduced to 50 km/h north of the landfill. Incorporating this change of speed limit into the model would reduce the impact at the sensitive receptors but would not change the resulting criterion. The exclusionary limit would still be used.

The gradient of the road near where Road 123 becomes Water Street is not level. If this information had been used, the impact of road noise on the local receptors would be higher which could potentially allow a higher impact at the PORs. This information was not used so the most conservative assessment was used.

Road Traffic could have been assessed further into the future but it would have been more likely to increase the limit that the Landfill would have to meet (i.e., more landfill noise would be allowed). To be conservative, only a 10 year horizon was assessed. This choice is the most conservative treatment.

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<sup>3</sup> Ornament – Ontario Road Noise Analysis Method for Environment and Transportation. Technical Document. Ministry of the Environment, October 1989, page 5.

## 2.4.2 On-Site Noise

The Current and five (5) *Alternative Method* worst-case noise emission scenarios, consisting of all relevant on-site noise sources listed above, operating simultaneously and at their maximum load, were modelled using Predictor software. Because the worst case for some of the Alternative Methods corresponds with other Alternative Methods, only the Current and three Alternative Methods were modelled. The worst case for Alternative Method 1 is the same as the Current model and Alternative Method 4 is the same as Alternative Method 5 model.

Predictor is a computer modelling program from Bruel and Kjaer, which follows the procedure specified by ISO standard 9613-2. As such, the prediction model takes into account the sound level attenuation of the entered sound power data with distance as well as any attenuation provided by building shielding and ground absorption.

### 2.4.2.1 Assumptions and Considerations

Operations may change with the seasons and staging of the landfill. To be conservative, worst-case scenarios have been modelled. Key assumptions are presented below:

- Peak activity (e.g., peak haul route traffic and all heavy equipment in use at the same time) was modelled for all scenarios.
- A ground absorption coefficient of 1.0 was used, as most of the ground between the sources and receptors is absorptive ground (i.e. grass).
- Default atmospheric conditions were used (i.e. temperature of 10°C and relative humidity of 70 %).
- Site topography (elevation contours) was incorporated into the noise model.
- For On-Site Truck Routes, the maximum hourly truck counts were used, and a travel speed of 20 km/hr.

### 2.4.3 Existing Noise Barriers

Berms were constructed as noise barriers when the facility was built. Those berms were imported into the noise model from elevation contours. From publically available aerial photography, street-level imagery and a site visit, no other noise barriers exist within the Study Area.

## 2.5 Results

The landfill only operates during the day and has no noise emissions during the night. As a result the daytime is the only time period assessed. The scenario used to model each option is very conservative. The scenario assumes that all the trucks expected at the facility in 1 day complete their deliveries in the same hour. In that same hour the compactor operates for the entire hour.

The purpose of these tables is to present the predicted daytime impact at sensitive PORs at both 1.5 m and 4.5 m that the applicable noise sources, identified as significant in the Noise Source Summary Table (Table 1-Exist), have on the identified points of reception (Table 2).

### **2.5.1 Existing Conditions**

Table 3-Exist: Point of Reception Noise Impact Table (Unmitigated Current) shows the Source ID, Source Type, Distance from the Source to Receptor, and the Sound Pressure Level predicted at each POR. The results are summarized in Table 4-Exist: Acoustic Assessment Summary Table: Daytime (Un-Mitigated Current).

### **2.5.2 Alternative Method 2: Horizontal Expansion**

Table 3-M2: Point of Reception Noise Impact Table (Unmitigated Method 2) shows the Source ID, Source Type, Distance from the Source to Receptor, and the Sound Pressure Level predicted at each POR. The results are summarized in Table 4-M2: Acoustic Assessment Summary Table: Daytime (Un-Mitigated Method 2).

### **2.5.3 Alternative Method 3: Vertical and Horizontal Expansion**

Table 3-M3: Point of Reception Noise Impact Table (Unmitigated Method 3) shows the Source ID, Source Type, Distance from the Source to Receptor, and the Sound Pressure Level predicted at each POR. The results are summarized in Table 4-M3: Acoustic Assessment Summary Table: Daytime (Un-Mitigated Method 3).

### **2.5.4 Alternative Method 5: Combination of Vertical Expansion and Development of a New Landfill Footprint**

Table 3-M5: Point of Reception Noise Impact Table (Unmitigated Method 5) shows the Source ID, Source Type, Distance from the Source to Receptor, and the Sound Pressure Level predicted at each POR. The results are summarized in Table 4-M5: Acoustic Assessment Summary Table: Daytime (Un-Mitigated Method 5).

## **2.6 Investigation of Noise Mitigation**

### **2.6.1 Noise Mitigation Measures**

Based on the completed noise assessment, the predicted noise impacts for the existing landfill, as well as all *Alternative Methods* are within the guidelines specified by the MOECC, and as a result, mitigation measures for noise are not required.



### 3.0 Comparison of Alternative Methods

The existing noise levels experienced at each POR are compared to the predicted noise levels in each *Alternative Method*. Table 5: Comparison of the Change in Sound Levels at Each POR, shows the existing noise level, and the change in noise level experienced at each POR for the three (3) different Alternative Methods.

The MOECC, in their document “Ontario Ministry of Environment and Energy (MOEE), 1994, *MOEE/GO Transit Noise and Vibration Protocol - December 1994 (Draft #9)*” characterize the difference in sound impacts as shown in the following table:

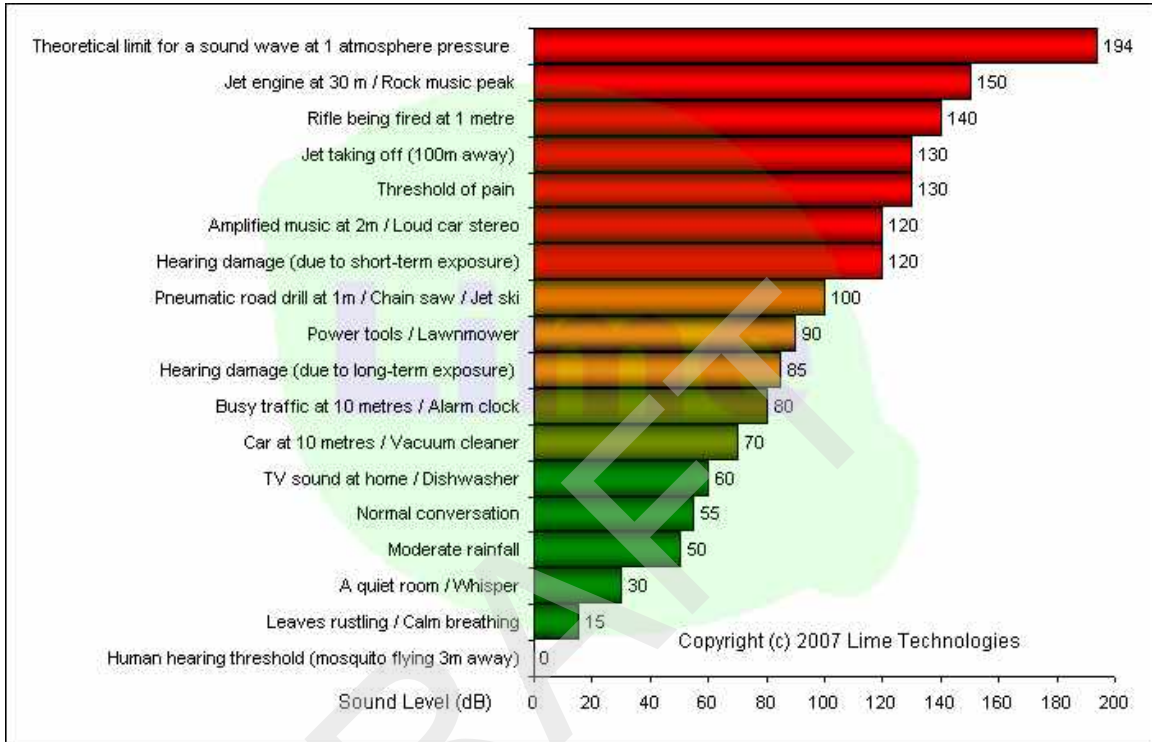
Table 3.1 Noise Impact Objectives

<b>Difference in sound level</b>	<b>Impact Rating</b>
0 to 2.99 dB	Insignificant
3.0 to 4.99 dB	Noticeable
5.0 to 9.99 dB	Significant
10+ dB	Very Significant

These levels were used to characterize the difference in sound level impact at the PORs as shown in Table 5: Comparison of the Change in Sound Levels at Each POR.

For reference, the following table is provided to understand the level of noise typical at various measured values.

Table 3.2 Typical Noise Levels



## 4.0 Vibration

Roads on-site are well graded and maintained. Vibration is not expected to be an issue from road traffic.

The compactor does not vibrate so vibration is not expected to be an issue from the compactor.

Ground-borne vibration generated by equipment expected at this facility is not detectable beyond 75 m. The closest receptor is approximately 150 m from the facility so even if there were significant sources of vibration at the facility they would not likely be detectable at the nearest sensitive receptors.

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## 5.0 Conclusion and Recommendations

The conclusions and recommendations based on the above analysis for the noise and vibration assessments are discussed below.

### 5.1 Conclusions

The first observation about these results is that the Current operation, assuming the worst noise emissions possible, shows compliance with the MOECC criteria of 55 dBA during the day. In fact, the highest modelled impact is 51 dBA at POR\_04\_B which is noticeably below the criterion.

The next observation is that under all five *Alternative Methods*, the noise impact at all receptors is also less than the MOECC criterion of 55 dBA. Some receptors show an increase in noise while others show a decrease but, in general, the increases are largest at locations that show an impact substantially below the criterion while the most impacted locations see a decrease. The most impacted receptor under *Alternative Method 3*, and 5 is POR\_03\_B at 50 dBA, unchanged from the Current impact; however, the previously most impacted location (POR\_04\_B) shows a reduction of 2-3 dBA.

Since all receptors meet the MOCEE criterion, mitigation measures for noise are not required.

Vibration is typically not felt further than 75 m from the source. The closest sensitive receptor is located 148.5 m from the landfill operations so vibration from delivery, placement, compaction and covering the waste within the expanded landfill was considered negligible.

### 5.2 Recommendations

Each *Alternative Method* meets the Ministry daytime criteria of 55 dB at all sensitive points of reception; therefore all five Methods are acceptable potential expansion options for the St. Marys landfill.

All five *Alternative Methods* will result in a reduction of noise at the most impacted receptors and the only significant increases are at receptors that currently show fairly low impacts. The increase will, at worst, result in an impact that is well below criterion.

None of the *Alternative Methods* is significantly better or worse than the others from a noise impact point of view.

## 6.0 References

Ontario Ministry of the Environment (MOE), 1995, Publication NPC-205, *Sound Level Limits for Stationary Sources in Class 1&2 Areas (Urban)*.

Ontario Ministry of Environment and Energy (MOEE), 1994, *MOEE/GO Transit Noise and Vibration Protocol - December 1994 (Draft #9)*.

Ontario Ministry of Environment (MOE), 2013, *Environmental Noise Guideline, Stationary and Transportation Sources – Approval and Planning, Publication NPC-300*.

Ontario Ministry of the Environment (MOE), 1998, *Noise Guidelines for Landfill Sites (DRAFT)*.

Ornament – Ontario Road Noise Analysis Method for Environment and Transportation. Technical Document. Ministry of the Environment, October 1989, page 5.

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## 7.0 Project Limitations and Caveats

The location of the on-site roads, open face and compactor that have been assessed for Alternative Method 2, 3 and 5 are the worst-case option for each method expansion.

Alternative Method 2, 3 and 5 are proposed landfill expansion options, and conceptual site plans outlining the location of the scale house, on-site roads, open face, and the compactor, have been used. The on-site roads, tipping face and compactor locations that have been assessed for each method are the worst-case scenario for each proposed expansion alternative. It is recognized that the on-site road routes and the location of the open face and the compactor may change from the modelled scenario; however, the impact at the PORs should remain the same, or have a decreased impact from the modelled result.

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## Tables

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Source ID	Source Description	Note <sup>A</sup>	Source Location <sup>B</sup>	Coordinates		Unmitigated Sound Power Level				
				X	Y	Lw	Day	Characteristic Penalty	Sound Char <sup>C</sup>	Noise Control Measures <sup>D</sup>
				(m)	(m)	(dBA)	(%)			
<b>Area Sources</b>										
CMPTR	1986 CAT 816D Compactor	2*	O	487259.5	4787100	106.3	100.0	0	S	U

Moving Sources	Source Description	Note <sup>A</sup>	Source Location <sup>B</sup>	Length	Avg. Speed	Lw	Trips/h	Characteristic Penalty	Sound Char <sup>C</sup>	Noise Control Measures <sup>D</sup>
				(m)	(km/h)	(dBA)	(Day)			
OnSiteTrk1	Entrance to Scale	2*	O	327.6	20.0	105.1	192.0	0	S	U
OnSiteTrk2	Scale to Open Face	2*	O	81.1	20.0	105.1	96.0	0	S	U
OnSiteTrk3	Travelling to Compost Area	2*	O	725.1	20.0	105.1	96.0	0	S	U
OnSiteTrk4	Travelling to Stock Pile	2*	O	400.2	20.0	105.1	48.0	0	S	U

**^Notes:**

1 - established from manufacturer's data

2 - established through on-Site measurements

3- established through correlations (see App. C)

2\*- established through measurements of similar sources at other Sites

<sup>B</sup>Source Location: O: Outside the building, I: Inside the building envelope<sup>C</sup>Sound Characteristics: S: Steady, Q: Quasi Steady Impulsive, I: Impulsive, B: Buzzing, T: Tonal, C: Cyclic<sup>D</sup>Noise Control Measures: S: Silencer, A: Acoustic Lining, plenum, B: Barrier, berm, screening, L: Lagging, E: Acoustic Enclosure, O: Other, U: Uncontrolled



Source ID	Source Description	Note <sup>A</sup>	Source Location <sup>B</sup>	Coordinates		Unmitigated Sound Power Level				
				X	Y	Lw	Day	Characteristic Penalty	Sound Char <sup>C</sup>	Noise Control Measures <sup>D</sup>
				(m)	(m)	(dBA)	(%)			
<b>Area Sources</b>										
CMPTR	1986 CAT 816D Compactor		O	487360	4787284.4	106.3	100.0	0	S	U

Moving Sources	Source Description	Note <sup>A</sup>	Source Location <sup>B</sup>	Length	Avg. Speed	Lw	Trips/h	Characteristic Penalty	Sound Char <sup>C</sup>	Noise Control Measures <sup>D</sup>
				(m)	(km/h)	(dBA)	(Day)			
OnSiteTrk1	Entrance to Scale	2*	O	327.6	20.0	105.1	192.0	0	S	U
OnSiteTrk2	Scale to Open Face	2*	O	230.1	20.0	105.1	96.0	0	S	U
OnSiteTrk3	Scale to Composte	2*	O	667.5	20.0	105.1	96.0	0	S	U
OnSiteTrk4	Scale to Stock Pile	2*	O	594.6	20.0	105.1	48.0	0	S	U

**^Notes:**

1 - established from manufacturer's data

2 - established through on-Site measurements

3- established through correlations (see App. C)

2\*- established through measurements of similar sources at other Sites

<sup>B</sup>Source Location: O: Outside the building, I: Inside the building envelope<sup>C</sup>Sound Characteristics: S: Steady, Q: Quasi Steady Impulsive, I: Impulsive, B: Buzzing, T: Tonal, C: Cyclic<sup>D</sup>Noise Control Measures: S: Silencer, A: Acoustic Lining, plenum, B: Barrier, berm, screening, L: Lagging, E: Acoustic Enclosure, O: Other, U: Uncontrolled

Source ID	Source Description	Note <sup>A</sup>	Source Location <sup>B</sup>	Coordinates		Unmitigated Sound Power Level				
				X	Y	Lw	Day	Characteristic Penalty	Sound Char <sup>C</sup>	Noise Control Measures <sup>D</sup>
				(m)	(m)	(dBA)	(%)			
<b>Area Sources</b>										
CMPTR	1986 CAT 816D Compactor		O	487228.7	4787206.8	106.3	100.0	0	S	U

Moving Sources		Note <sup>A</sup>	Source Location <sup>B</sup>	Length	Avg. Speed	Lw	Trips/h	Characteristic Penalty	Sound Char <sup>C</sup>	Noise Control Measures <sup>D</sup>
				(m)	(km/h)	(dBA)	(Day)			
OnSiteTrk1	Entrance to Scale	2*	O	271.1	20.0	105.1	192.0	0	S	U
OnSiteTrk2	Scale to Open Face	2*	O	68.3	20.0	105.1	96.0	0	S	U
OnSiteTrk3	Scale to Compost	2*	O	534.6	20.0	105.1	96.0	0	S	U
OnSiteTrk4	Scale to Stock Pile	2*	O	515.5	20.0	105.1	48.0	0	S	U

**^Notes:**

1 - established from manufacturer's data

2 - established through on-Site measurements

3 - established through correlations (see App. C)

2\* - established through measurements of similar sources at other Sites

<sup>B</sup>Source Location: O: Outside the building, I: Inside the building envelope<sup>C</sup>Sound Characteristics: S: Steady, Q: Quasi Steady Impulsive, I: Impulsive, B: Buzzing, T: Tonal, C: Cyclic<sup>D</sup>Noise Control Measures: S: Silencer, A: Acoustic Lining, plenum, B: Barrier, berm, screening, L: Lagging, E: Acoustic Enclosure, O: Other, U: Uncontrolled

Source ID	Source Description	Note <sup>A</sup>	Source Location <sup>B</sup>	Coordinates		Unmitigated Sound Power Level				
				X	Y	Lw	Day	Characteristic Penalty	Sound Char <sup>C</sup>	Noise Control Measures <sup>D</sup>
				(m)	(m)	(dBA)	(%)			
<b>Area Sources</b>										
CMPTR	1986 CAT 816D Compactor		O	487228.7	4787206.8	106.3	100.0	0	S	U

Moving Sources	Source Description	Note <sup>A</sup>	Source Location <sup>B</sup>	Length	Avg. Speed	Lw	Trips/h	Characteristic Penalty	Sound Char <sup>C</sup>	Noise Control Measures <sup>D</sup>
OnSiteTrk1	Entrance to Scale	2*	O	252.3	20.0	105.1	192.0	0	S	U
OnSiteTrk2	Scale to Open Face	2*	O	50.2	20.0	105.1	96.0	0	S	U
OnSiteTrk3	Scale to Composte	2*	O	662.9	20.0	105.1	96.0	0	S	U
OnSiteTrk4	Scale to Stock Pile	2*	O	630.6	20.0	105.1	48.0	0	S	U

<sup>A</sup>Notes:

1 - established from manufacturer's data

2 - established through on-Site measurements

3- established through correlations (see App. C)

2\*- established through measurements of similar sources at other Sites

<sup>B</sup>Source Location: O: Outside the building, I: Inside the building envelope<sup>C</sup>Sound Characteristics: S: Steady, Q: Quasi Steady Impulsive, I: Impulsive, B: Buzzing, T: Tonal, C: Cyclic<sup>D</sup>Noise Control Measures: S: Silencer, A: Acoustic Lining, plenum, B: Barrier, berm, screening, L: Lagging, E: Acoustic Enclosure, O: Other, U: Uncontrolled

POR	POR Description	POR Location	UTM X Coordinate	UTM Y Coordinate	Height (m)	Basis of Criteria	Day 0700 - 1900	Evening 1900 - 2300	Night 2300 - 0700	Receptor Type (OLA/POW)
POR_01_A	Two Storey Residential House	1025 Water Street South	487216	4787437	1.5	MOE Noise Guidelines for Landfill	55	45	45	POW
POR_01_B	Two Storey Residential House	1025 Water Street South	487216	4787437	4.5	MOE Noise Guidelines for Landfill	55	45	45	POW
POR_02_A	Two Storey Residential House	1774 Water Street South	487082	4787408	1.5	MOE Noise Guidelines for Landfill	55	45	45	POW
POR_02_B	Two Storey Residential House	1774 Water Street South	487082	4787408	4.5	MOE Noise Guidelines for Landfill	55	45	45	POW
POR_03_A	One Storey Residential House	1827 Water Street South	487091	4787111	1.5	MOE Noise Guidelines for Landfill	55	45	45	POW
POR_03_B	One Storey Residential House	1827 Water Street South	487091	4787111	4.5	MOE Noise Guidelines for Landfill	55	45	45	POW
POR_04_A	Two Storey Residential House	4461 3 Line	487135	4786936	1.5	MOE Noise Guidelines for Landfill	55	45	45	POW
POR_04_B	Two Storey Residential House	4461 3 Line	487135	4786936	4.5	MOE Noise Guidelines for Landfill	55	45	45	POW
POR_05_A	Two Storey Residential House	1646 Perth Road 123	487185	4786617	1.5	MOE Noise Guidelines for Landfill	55	45	45	POW
POR_05_B	Two Storey Residential House	1646 Perth Road 123	487185	4786617	4.5	MOE Noise Guidelines for Landfill	55	45	45	POW
POR_06_A	Two Storey Residential House	1579 Perth Road 123	487326	4786203	1.5	MOE Noise Guidelines for Landfill	55	45	45	POW
POR_06_B	Two Storey Residential House	1579 Perth Road 123	487326	4786203	4.5	MOE Noise Guidelines for Landfill	55	45	45	POW

Source ID	Source Type	POR_04_A		POR_04_B		POR_03_A		POR_03_B		POR_02_A		POR_02_B	
		Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)
CMPTR	Area	205.9	45.0	205.9	47.9	168.9	44.1	168.9	48.5	355.5	38.3	355.5	41.6
OnSiteTrk1	Moving	208.9	44.8	208.9	46.6	126.0	42.3	126.0	44.2	309.7	32.9	309.7	35.0
OnSiteTrk2	Moving	206.5	28.4	206.5	30.5	127.3	30.2	127.3	32.3	313.4	22.0	313.4	25.9
OnSiteTrk3	Moving	210.4	31.4	210.4	35.1	131.2	32.5	131.2	36.1	312.7	29.1	312.7	32.7
OnSiteTrk4	Moving	209.3	28.9	209.3	32.3	132.6	29.6	132.6	33.1	315.1	25.0	315.1	28.9
<b>TOTAL</b>			48.1		50.6		46.7		50.2		40.0		43.1
<b>Rounded TOTAL</b>			48		51		47		50		40		43

<sup>1</sup>The distance to the POR from non-Point Sources is calculated from the first node in the source.

Source ID	Source Type	POR_05_A		POR_05_B		POR_06_A		POR_06_B		POR_01_A		POR_01_B	
		Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)
CMPTR	Area	488.7	34.4	488.7	38.0	899.4	27.3	899.4	27.8	339.8	26.9	339.8	29.5
OnSiteTrk1	Moving	512.6	32.3	512.6	34.5	932.2	24.3	932.2	26.7	308.3	21.0	308.3	24.9
OnSiteTrk2	Moving	509.4	18.9	509.4	21.1	928.7	12.4	928.7	13.2	311.6	11.5	311.6	15.5
OnSiteTrk3	Moving	512.2	25.9	512.2	27.2	930.9	21.2	930.9	22.1	309.1	20.0	309.1	22.6
OnSiteTrk4	Moving	510.4	21.8	510.4	24.4	928.8	16.0	928.8	17.3	311.0	15.1	311.0	18.4
<b>TOTAL</b>			37.0		40.0		30.0		31.2		28.8		31.7
<b>Rounded TOTAL</b>			37		40		30		31		29		32

<sup>1</sup>The distance to the POR from non-Point Sources is calculated from the first node in the source.

Source ID	Source Type	POR_04_A		POR_04_B		POR_03_A		POR_03_B		POR_02_A		POR_02_B	
		Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)
CMPTR	Area	414.7	40.3	205.9	41.2	168.9	42.1	168.9	43.4	355.5	43.0	355.5	43.4
OnSiteTrk1	Moving	208.9	45.3	208.9	47.0	126.0	42.8	126.0	44.5	309.7	33.9	309.7	35.6
OnSiteTrk2	Moving	203.5	31.2	206.5	33.5	127.3	33.5	127.3	36.8	313.4	31.3	313.4	33.4
OnSiteTrk3	Moving	222.8	31.2	210.4	33.5	131.2	33.7	131.2	37.8	312.7	35.1	312.7	37.0
OnSiteTrk4	Moving	222.3	28.7	209.3	30.8	132.6	30.9	132.6	34.0	315.1	31.7	315.1	33.8
<b>TOTAL</b>			46.8		48.3		46.2		48.0		44.5		45.5
<b>Rounded TOTAL</b>			47		48		46		48		45		46

<sup>1</sup>The distance to the POR from non-Point Sources is calculated from the first node in the source.

Source ID	Source Type	POR_05_A		POR_05_B		POR_06_A		POR_06_B		POR_01_A		POR_01_B	
		Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)
CMPTR	Area	488.7	32.9	488.7	35.2	899.4	26.6	899.4	28.8	339.8	28.9	339.8	31.5
OnSiteTrk1	Moving	512.6	33.0	512.6	35.0	932.2	25.1	932.2	27.3	308.3	23.2	308.3	26.3
OnSiteTrk2	Moving	509.4	23.2	509.4	25.8	928.7	15.8	928.7	19.9	311.6	21.3	311.6	23.6
OnSiteTrk3	Moving	512.2	24.7	512.2	27.6	930.9	19.4	930.9	22.0	309.1	24.3	309.1	27.1
OnSiteTrk4	Moving	510.4	21.6	510.4	24.7	928.8	16.1	928.8	18.8	311.0	21.0	311.0	23.9
<b>TOTAL</b>			36.6		38.8		29.7		32.1		31.8		34.5
<b>Rounded TOTAL</b>			37		39		30		32		32		35

<sup>1</sup>The distance to the POR from non-Point Sources is calculated from the first node in the source.



Source ID	Source Type	POR_04_A		POR_04_B		POR_03_A		POR_03_B		POR_02_A		POR_02_B	
		Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)
CMPTR	Area	286.6	43.3	205.9	44.0	168.9	48.0	168.9	48.5	355.5	45.0	355.5	45.6
OnSiteTrk1	Moving	84.3	44.3	208.9	46.2	126.0	39.9	126.0	42.4	309.7	31.4	309.7	34.1
OnSiteTrk2	Moving	224.7	27.6	206.5	29.7	127.3	33.6	127.3	35.5	313.4	27.4	313.4	29.4
OnSiteTrk3	Moving	221.0	29.0	210.4	31.2	131.2	34.8	131.2	36.4	312.7	33.0	312.7	34.5
OnSiteTrk4	Moving	256.1	25.8	209.3	27.9	132.6	28.8	132.6	30.2	315.1	29.3	315.1	30.6
<b>TOTAL</b>			47.0		48.4		49.0		49.9		45.6		46.4
<b>Rounded TOTAL</b>			47		48		49		50		46		46

<sup>1</sup>The distance to the POR from non-Point Sources is calculated from the first node in the source.

Source ID	Source Type	POR_05_A		POR_05_B		POR_06_A		POR_06_B		POR_01_A		POR_01_B	
		Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)
CMPTR	Area	488.7	35.6	488.7	36.4	899.4	29.3	899.4	30.4	339.8	36.9	339.8	38.3
OnSiteTrk1	Moving	512.6	31.7	512.6	33.9	932.2	23.6	932.2	26.3	308.3	20.8	308.3	24.0
OnSiteTrk2	Moving	509.4	19.2	509.4	21.5	928.7	12.6	928.7	15.0	311.6	19.5	311.6	22.8
OnSiteTrk3	Moving	512.2	22.9	512.2	24.1	930.9	18.4	930.9	19.9	309.1	25.0	309.1	28.5
OnSiteTrk4	Moving	510.4	19.8	510.4	21.3	928.8	15.6	928.8	17.4	311.0	21.5	311.0	25.0
<b>TOTAL</b>			37.4		38.7		30.8		32.3		37.4		39.1
<b>Rounded TOTAL</b>			37		39		31		32		37		39

<sup>1</sup>The distance to the POR from non-Point Sources is calculated from the first node in the source.

Source ID	Source Type	POR_04_A		POR_04_B		POR_03_A		POR_03_B		POR_02_A		POR_02_B	
		Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)
CMPTR	Area	286.6	44.1	205.9	44.7	168.9	48.5	168.9	49.0	355.5	44.3	355.5	44.9
OnSiteTrk1	Moving	84.3	44.0	208.9	45.9	126.0	40.6	126.0	43.3	309.7	31.7	309.7	34.1
OnSiteTrk2	Moving	224.7	26.0	206.5	28.0	127.3	32.3	127.3	34.1	313.4	26.1	313.4	28.0
OnSiteTrk3	Moving	221.0	29.0	210.4	31.6	131.2	34.0	131.2	36.4	312.7	34.5	312.7	36.5
OnSiteTrk4	Moving	256.1	28.0	209.3	30.1	132.6	32.2	132.6	34.6	315.1	31.9	315.1	33.9
<b>TOTAL</b>			47.2		48.6		49.4		50.4		45.2		46.1
<b>Rounded TOTAL</b>			<b>47</b>		<b>49</b>		<b>49</b>		<b>50</b>		<b>45</b>		<b>46</b>

<sup>1</sup>The distance to the POR from non-Point Sources is calculated from the first node in the source.

Source ID	Source Type	POR_05_A		POR_05_B		POR_06_A		POR_06_B		POR_01_A		POR_01_B	
		Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)	Distance (m) <sup>1</sup>	Sound Pressure Level Leq in dBA (Day)
CMPTR	Area	488.7	36.0	488.7	36.8	899.4	29.6	899.4	30.6	339.8	34.8	339.8	36.2
OnSiteTrk1	Moving	512.6	31.1	512.6	33.3	932.2	23.3	932.2	25.9	308.3	21.5	308.3	24.2
OnSiteTrk2	Moving	509.4	17.5	509.4	19.7	928.7	11.6	928.7	14.2	311.6	17.9	311.6	22.0
OnSiteTrk3	Moving	512.2	23.4	512.2	25.4	930.9	19.4	930.9	20.5	309.1	25.7	309.1	29.3
OnSiteTrk4	Moving	510.4	21.8	510.4	24.0	928.8	17.0	928.8	18.8	311.0	23.1	311.0	26.2
<b>TOTAL</b>			37.5		38.8		31.1		32.4		35.8		37.7
<b>Rounded TOTAL</b>			<b>38</b>		<b>39</b>		<b>31</b>		<b>32</b>		<b>36</b>		<b>38</b>

<sup>1</sup>The distance to the POR from non-Point Sources is calculated from the first node in the source.

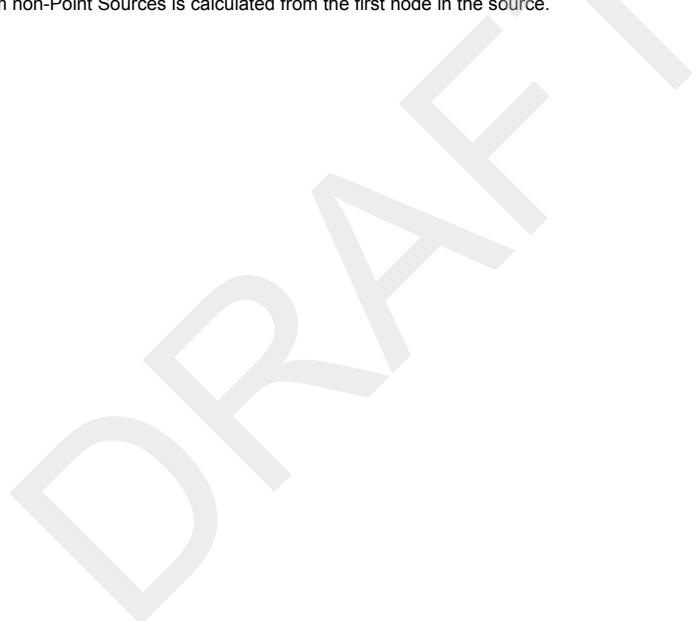


Table 4-Exist: Acoustic Assessment Summary Table: Daytime (Un-Mitigated Current)

Point of Reception ID	Point of Reception Description	Height (m)	Sound Level at Point of Reception (Leq)(dBA)	Verified by an Acoustic Audit (Yes/No)	Performance Limit (0700h-1900h) (LAeq)	Compliance with Performance Limit (Yes / No)
POR_01_A	Two Storey Residential House (POW)	1.5	29	No	55	Yes
POR_01_B	Two Storey Residential House (POW)	4.5	32	No	55	Yes
POR_02_A	Two Storey Residential House (POW)	1.5	40	No	55	Yes
POR_02_B	Two Storey Residential House (POW)	4.5	43	No	55	Yes
POR_03_A	One Storey Residential House (POW)	1.5	47	No	55	Yes
POR_03_B	One Storey Residential House (POW)	4.5	50	No	55	Yes
POR_04_A	Two Storey Residential House (POW)	1.5	48	No	55	Yes
POR_04_B	Two Storey Residential House (POW)	4.5	51	No	55	Yes
POR_05_A	Two Storey Residential House (POW)	1.5	37	No	55	Yes
POR_05_B	Two Storey Residential House (POW)	4.5	40	No	55	Yes
POR_06_A	Two Storey Residential House (POW)	1.5	30	No	55	Yes
POR_06_B	Two Storey Residential House (POW)	4.5	31	No	55	Yes

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Table 4-M2: Acoustic Assessment Summary Table: Daytime (Un-Mitigated Method 2)

Point of Reception ID	Point of Reception Description	Height (m)	Sound Level at Point of Reception (Leq)(dBA)	Verified by an Acoustic Audit (Yes/No)	Performance Limit (0700h-1900h) (LAeq)	Compliance with Performance Limit (Yes / No)
POR_01_A	Two Storey Residential House (POW)	1.5	32	No	55	Yes
POR_01_B	Two Storey Residential House (POW)	4.5	35	No	55	Yes
POR_02_A	Two Storey Residential House (POW)	1.5	45	No	55	Yes
POR_02_B	Two Storey Residential House (POW)	4.5	46	No	55	Yes
POR_03_A	One Storey Residential House (POW)	1.5	46	No	55	Yes
POR_03_B	One Storey Residential House (POW)	4.5	48	No	55	Yes
POR_04_A	Two Storey Residential House (POW)	1.5	47	No	55	Yes
POR_04_B	Two Storey Residential House (POW)	4.5	48	No	55	Yes
POR_05_A	Two Storey Residential House (POW)	1.5	37	No	55	Yes
POR_05_B	Two Storey Residential House (POW)	4.5	39	No	55	Yes
POR_06_A	Two Storey Residential House (POW)	1.5	30	No	55	Yes
POR_06_B	Two Storey Residential House (POW)	4.5	32	No	55	Yes

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Table 4-M3: Acoustic Assessment Summary Table: Daytime (Un-Mitigated Method 3)

Point of Reception ID	Point of Reception Description	Height (m)	Sound Level at Point of Reception (Leq)(dBA)	Verified by an Acoustic Audit (Yes/No)	Performance Limit (0700h-1900h) (LAeq)	Compliance with Performance Limit (Yes / No)
POR_01_A	Two Storey Residential House (POW)	1.5	37	No	55	Yes
POR_01_B	Two Storey Residential House (POW)	4.5	39	No	55	Yes
POR_02_A	Two Storey Residential House (POW)	1.5	46	No	55	Yes
POR_02_B	Two Storey Residential House (POW)	4.5	46	No	55	Yes
POR_03_A	One Storey Residential House (POW)	1.5	49	No	55	Yes
POR_03_B	One Storey Residential House (POW)	4.5	50	No	55	Yes
POR_04_A	Two Storey Residential House (POW)	1.5	47	No	55	Yes
POR_04_B	Two Storey Residential House (POW)	4.5	48	No	55	Yes
POR_05_A	Two Storey Residential House (POW)	1.5	37	No	55	Yes
POR_05_B	Two Storey Residential House (POW)	4.5	39	No	55	Yes
POR_06_A	Two Storey Residential House (POW)	1.5	31	No	55	Yes
POR_06_B	Two Storey Residential House (POW)	4.5	32	No	55	Yes

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Table 4-M5: Acoustic Assessment Summary Table: Daytime (Un-Mitigated Method 5)

Point of Reception ID	Point of Reception Description	Height (m)	Sound Level at Point of Reception (Leq)(dBA)	Verified by an Acoustic Audit (Yes/No)	Performance Limit (0700h-1900h) (LAeq)	Compliance with Performance Limit (Yes / No)
POR_01_A	Two Storey Residential House (POW)	1.5	36	No	55	Yes
POR_01_B	Two Storey Residential House (POW)	4.5	38	No	55	Yes
POR_02_A	Two Storey Residential House (POW)	1.5	45	No	55	Yes
POR_02_B	Two Storey Residential House (POW)	4.5	46	No	55	Yes
POR_03_A	One Storey Residential House (POW)	1.5	49	No	55	Yes
POR_03_B	One Storey Residential House (POW)	4.5	50	No	55	Yes
POR_04_A	Two Storey Residential House (POW)	1.5	47	No	55	Yes
POR_04_B	Two Storey Residential House (POW)	4.5	49	No	55	Yes
POR_05_A	Two Storey Residential House (POW)	1.5	38	No	55	Yes
POR_05_B	Two Storey Residential House (POW)	4.5	39	No	55	Yes
POR_06_A	Two Storey Residential House (POW)	1.5	31	No	55	Yes
POR_06_B	Two Storey Residential House (POW)	4.5	32	No	55	Yes

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POR#	Existing Conditions (dBA)	Alternative Method 2 (dBA)	Increase (+) OR Decrease (-) in dBA	Significant/ Insignificant <sup>1</sup>
POR_01_A	29	32	3	Noticeable
POR_01_B	32	35	3	Noticeable
POR_02_A	40	45	5	Significant
POR_02_B	43	46	3	Noticeable
POR_03_A	47	46	-1	Negligible
POR_03_B	50	48	-2	Negligible
POR_04_A	48	47	-1	Negligible
POR_04_B	51	48	-3	Negligible
POR_05_A	37	37	0	Negligible
POR_05_B	40	39	-1	Negligible
POR_06_A	30	30	0	Negligible
POR_06_B	31	32	1	Negligible

POR#	Existing Conditions (dBA)	Alternative Method 3 (dBA)	Increase (+) OR Decrease (-) in dBA	Significant/ Insignificant <sup>1</sup>
POR_01_A	29	37	8	Significant
POR_01_B	32	39	7	Significant
POR_02_A	40	46	6	Significant
POR_02_B	43	46	3	Noticeable
POR_03_A	47	49	2	Negligible
POR_03_B	50	50	0	Negligible
POR_04_A	48	47	-1	Negligible
POR_04_B	51	48	-3	Negligible
POR_05_A	37	37	0	Negligible
POR_05_B	40	39	-1	Negligible
POR_06_A	30	31	1	Negligible
POR_06_B	31	32	1	Negligible

POR#	Existing Conditions (dBA)	Alternative Method 5 (dBA)	Increase (+) OR Decrease (-) in dBA	Significant/ Insignificant <sup>1</sup>
POR_01_A	29	36	7	Significant
POR_01_B	32	38	6	Significant
POR_02_A	40	45	5	Significant
POR_02_B	43	46	3	Noticeable
POR_03_A	47	49	2	Negligible
POR_03_B	50	50	0	Negligible
POR_04_A	48	47	-1	Negligible
POR_04_B	51	49	-2	Negligible
POR_05_A	37	38	1	Negligible
POR_05_B	40	39	-1	Negligible
POR_06_A	30	31	1	Negligible
POR_06_B	31	32	1	Negligible

<sup>1</sup> Ontario Ministry of Environment and Energy (MOEE), 1994, *MOEE/GO Transit Noise and Vibration Protocol - December 1994 (Draft #9)*



# BURNSIDE

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## Figures

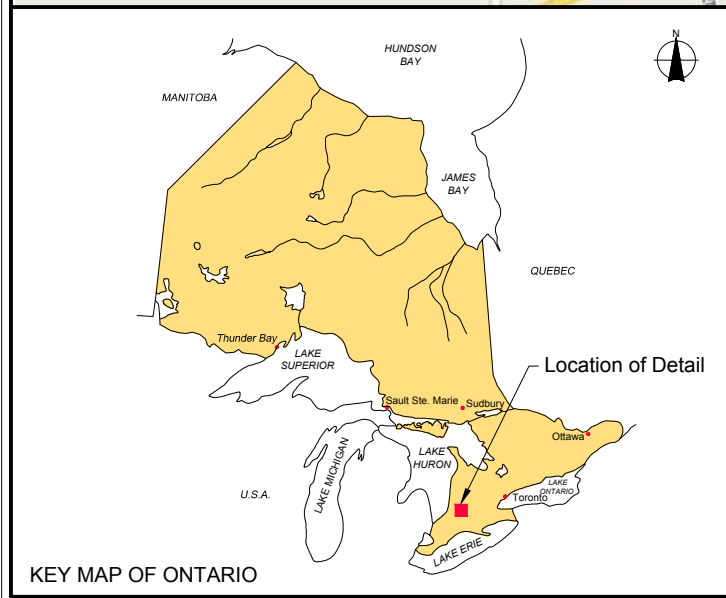
Figures

- Figure 1: Site Location
- Figure 2: Zoning
- Figure 3 – Exist: Site Plan Current
- Figure 3-M2: Site Plan Alternative Method 2
- Figure 3-M3: Site Plan Alternative Method 3
- Figure 3-M5: Site Plan Alternative Method 5
- Figure 4-Exist: Noise Contours Current
- Figure 4-M2: Noise Contours Alternative Method 2
- Figure 4-M3: Noise Contours Alternative Method 3
- Figure 4-M5: Noise Contours Alternative Method 5




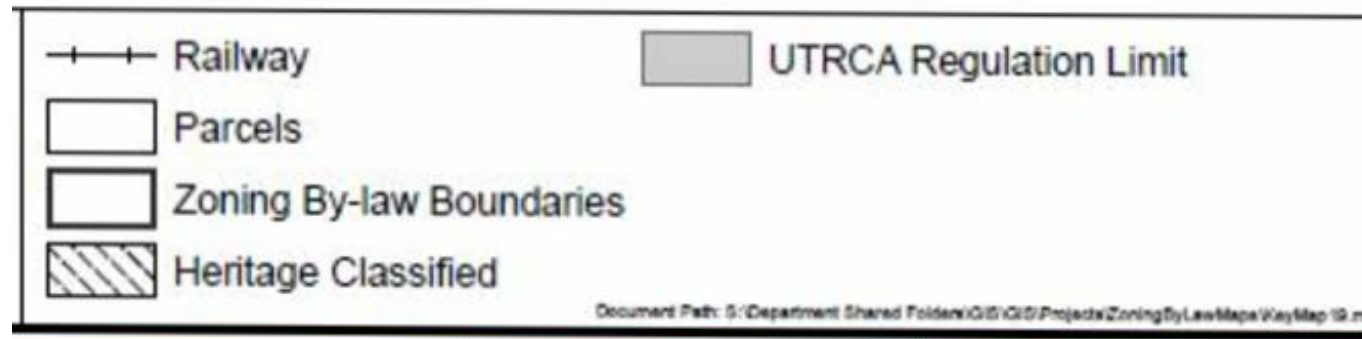
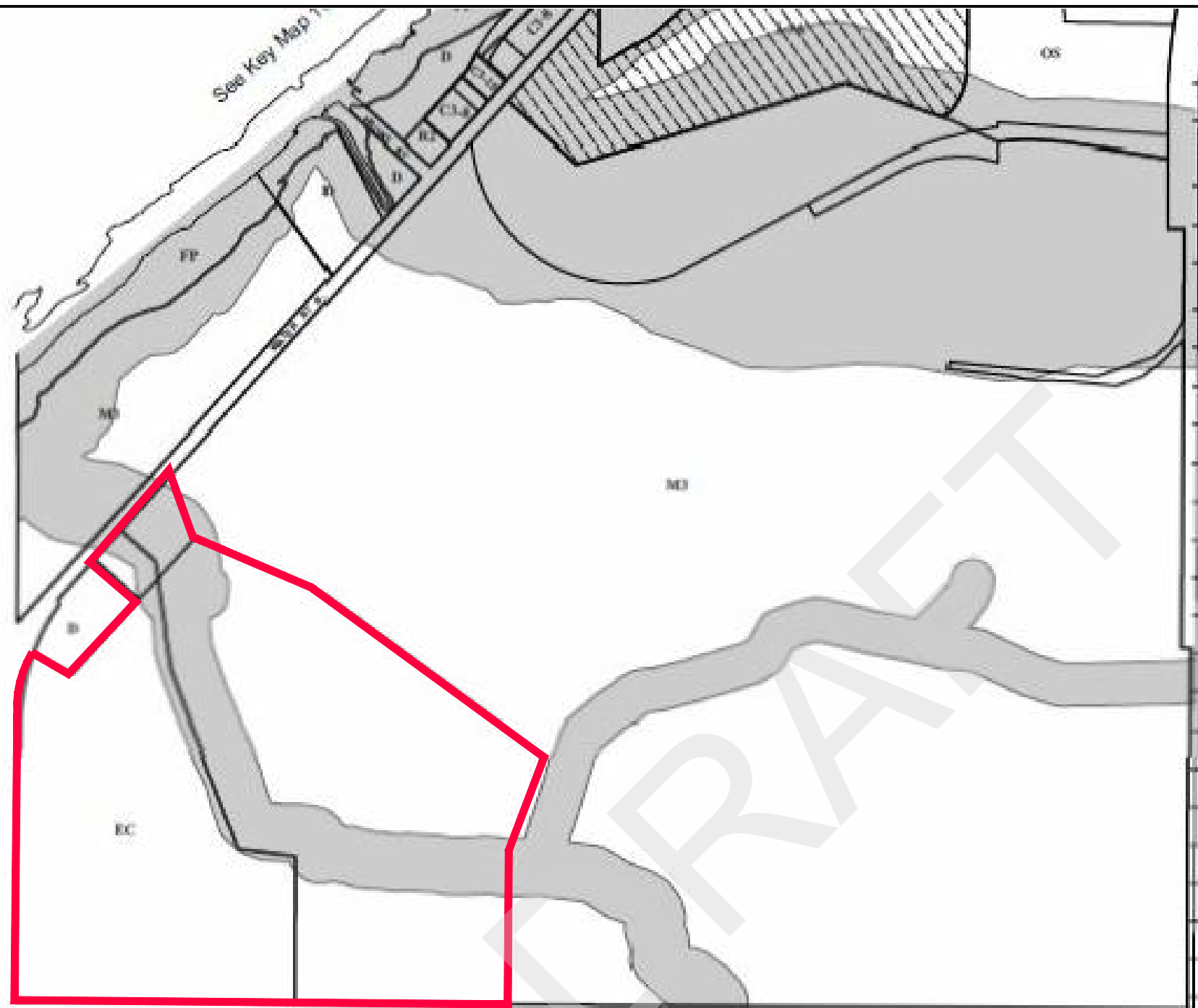
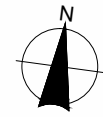
**Map Source:**

Background map obtained from Google Earth Professional.  
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KEY MAP OF ONTARIO

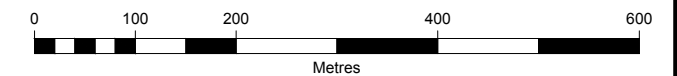
			
Client			
<b>CORPORATION OF THE TOWN OF ST. MARYS</b>			
Figure Title			
<b>ENVIRONMENTAL ASSESSMENT</b>			
SITE LOCATION MAP			
Drawn	Checked	Date	<b>1</b>
C.S.	H.W.	MARCH 2016	
Scale		Project No.	
1:25,000		300032339	



**LEGEND**

APPROXIMATE SITE BOUNDARY

Zone	Zone Symbol
Agricultural Zone One	A1
Agricultural Zone Two	A2
Residential Zone One	R1
Residential Zone Two	R2
Residential Zone Three	R3
Residential Zone Four	R4
Residential Zone Five	R5
Residential Zone Six	R6
Residential Zone Seven	R7
Central Commercial Zone	C1
Limited Commercial Zone	C2
Highway Commercial Zone	C3
Special Commercial Zone	C4
Light Industrial Zone	M1
General Industrial Zone	M2
Extractive Industrial Zone	M3
Environmental Constraint Zone	EC
Institutional Zone	I
Open Space Zone	OS
Flood Plain Zone	FP
Special Policy Area Constraint Zone	-SPA
Holding Zone	-H
Development Zone	D or RD



Zoning Map Source:  
Background zoning map obtained from the Corporation of the Town of St. Marys website. Zoning Map 19 from Zoning By-Law Z1-1997 consolidated through to January 15, 2015.



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Figure Title  
**ENVIRONMENTAL ASSESSMENT**

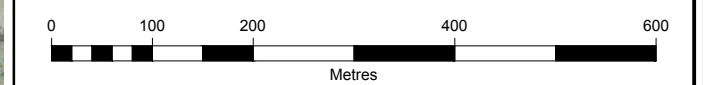
**ZONING LAND USE PLAN**

Drawn C.S.	Checked H.W.	Date MARCH 2016	Figure No. <b>2</b>
Scale 1:7,500	Project No. 300032339		




**LEGEND**

-  APPROXIMATE SITE BOUNDARY
-  POINT OF NOISE RECEPTION
-  POINT OF EMISSION
-  BOUNDARY COORDINATES  
X, Y = 568472  
4829089
-  EXISTING ON-SITE ROADS
-  EXISTING ON-SITE ROADS END POINTS



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Figure Title

**ENVIRONMENTAL ASSESSMENT**

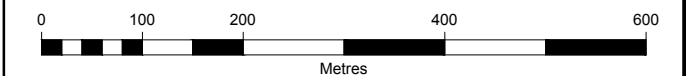
**SITE PLAN**  
**CURRENT CONDITIONS**

Drawn C.S.	Checked H.W.	Date MARCH 2016	Figure No.
Scale 1:7,500	Project No. 300032339		3-Exist



**LEGEND**

- APPROXIMATE SITE BOUNDARY
- POINT OF NOISE RECEPTION
- ▲ POINT OF EMISSION
- BOUNDARY COORDINATES  
X,Y = 568472  
4829089
- EXISTING ON-SITE ROADS
- EXISTING ON-SITE ROADS END POINTS
- PROPOSED LANDFILL EXPANSION



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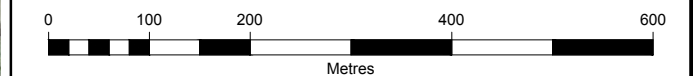
Figure Title  
**ENVIRONMENTAL ASSESSMENT  
POTENTIAL WASTE FILL AREA  
ALTERNATIVE #2**

Drawn C.S.	Checked H.W.	Date MARCH 2016	Figure No. <b>3-M2</b>
Scale 1:7,500	Project No. 300032339		




**LEGEND**

- APPROXIMATE SITE BOUNDARY
- POINT OF NOISE RECEPTION
- ▲ POINT OF EMISSION
- BOUNDARY COORDINATES  
X,Y = 568472  
4829089
- EXISTING ON-SITE ROADS
- A - G EXISTING ON-SITE ROADS END POINTS
- PROPOSED LANDFILL EXPANSION



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Figure Title

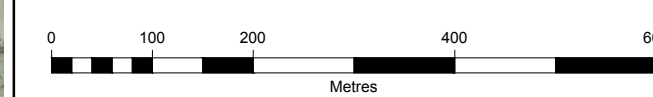
**ENVIRONMENTAL ASSESSMENT  
POTENTIAL WASTE FILL AREA  
ALTERNATIVE #3**

---


Drawn C.S.	Checked H.W.	Date MARCH 2016	Figure No.
Scale 1:7,500	Project No. 300032339		<b>3-M3</b>



- LEGEND**
- APPROXIMATE SITE BOUNDARY
  - POINT OF NOISE RECEPTION
  - ▲ POINT OF EMISSION
  - BOUNDARY COORDINATES  
X,Y = 568472  
4829089
  - EXISTING ON-SITE ROADS
  - A - G EXISTING ON-SITE ROADS END POINTS
  - PROPOSED LANDFILL EXPANSION



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**CORPORATION OF THE  
TOWN OF ST. MARYS**

---

Figure Title

**ENVIRONMENTAL ASSESSMENT  
POTENTIAL WASTE FILL AREA  
ALTERNATIVE #5**

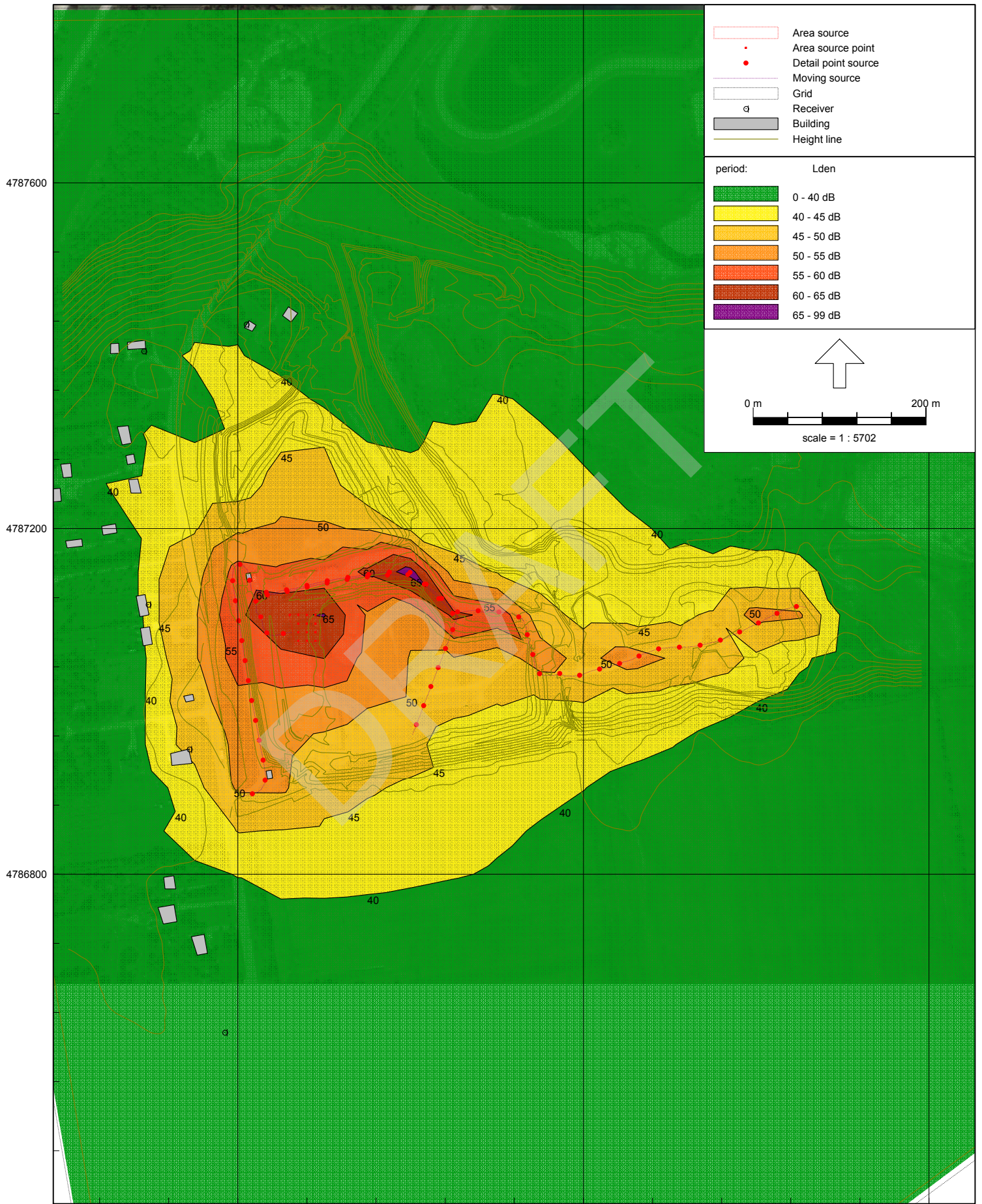
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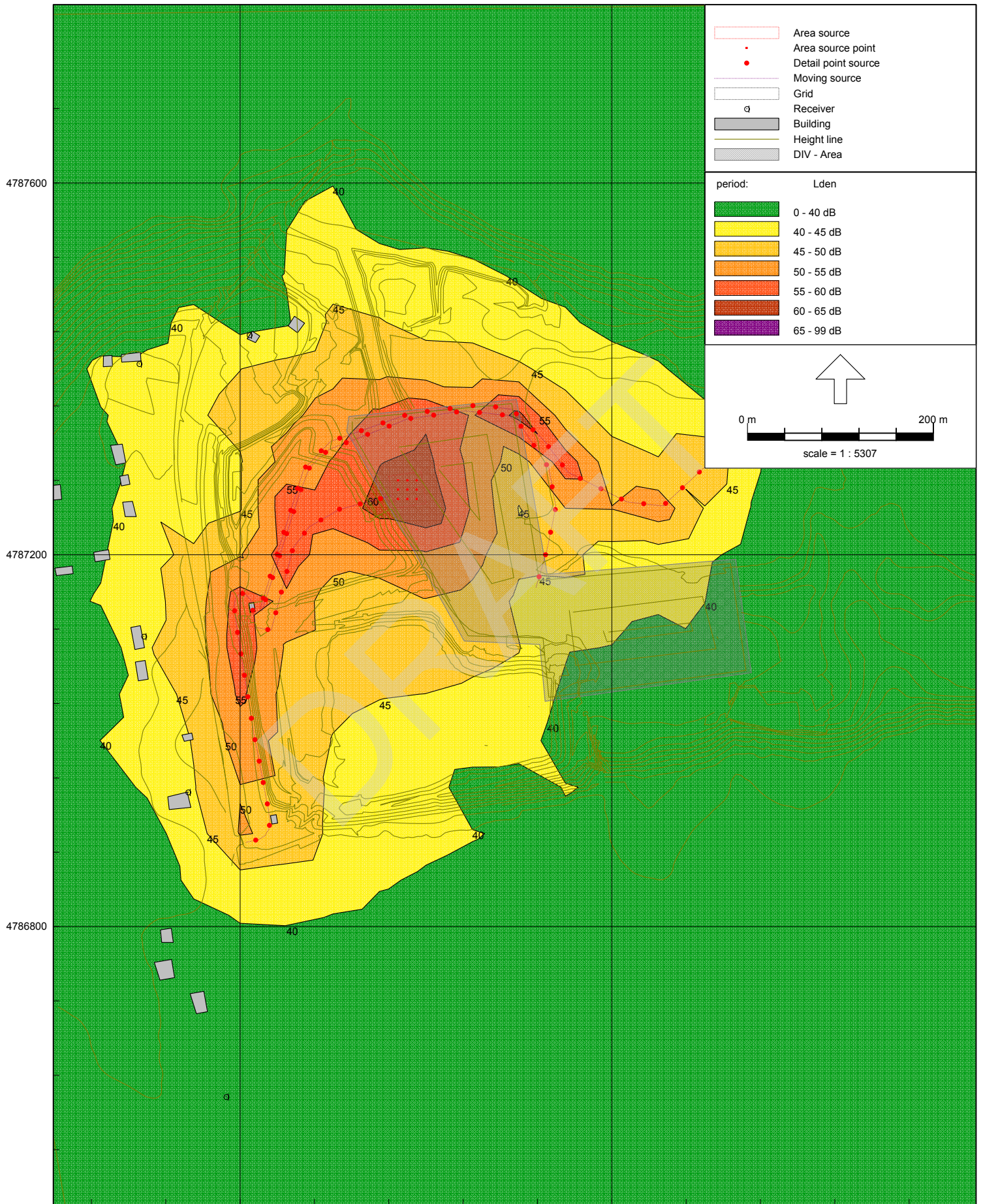
Drawn C.S.	Checked H.W.	Date MARCH 2016	Figure No.
Scale 1:7,500	Project No. 300032339		3-M5

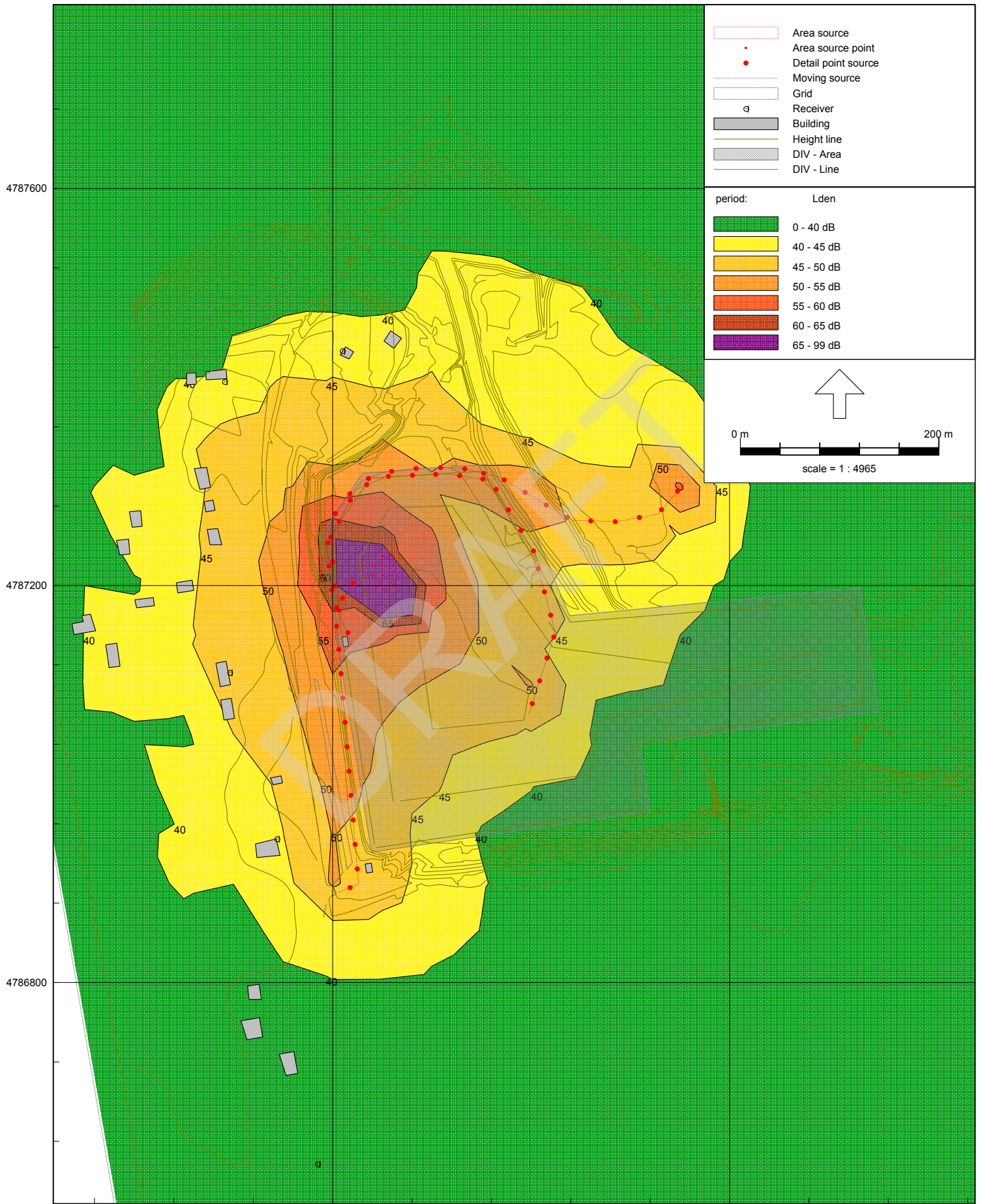


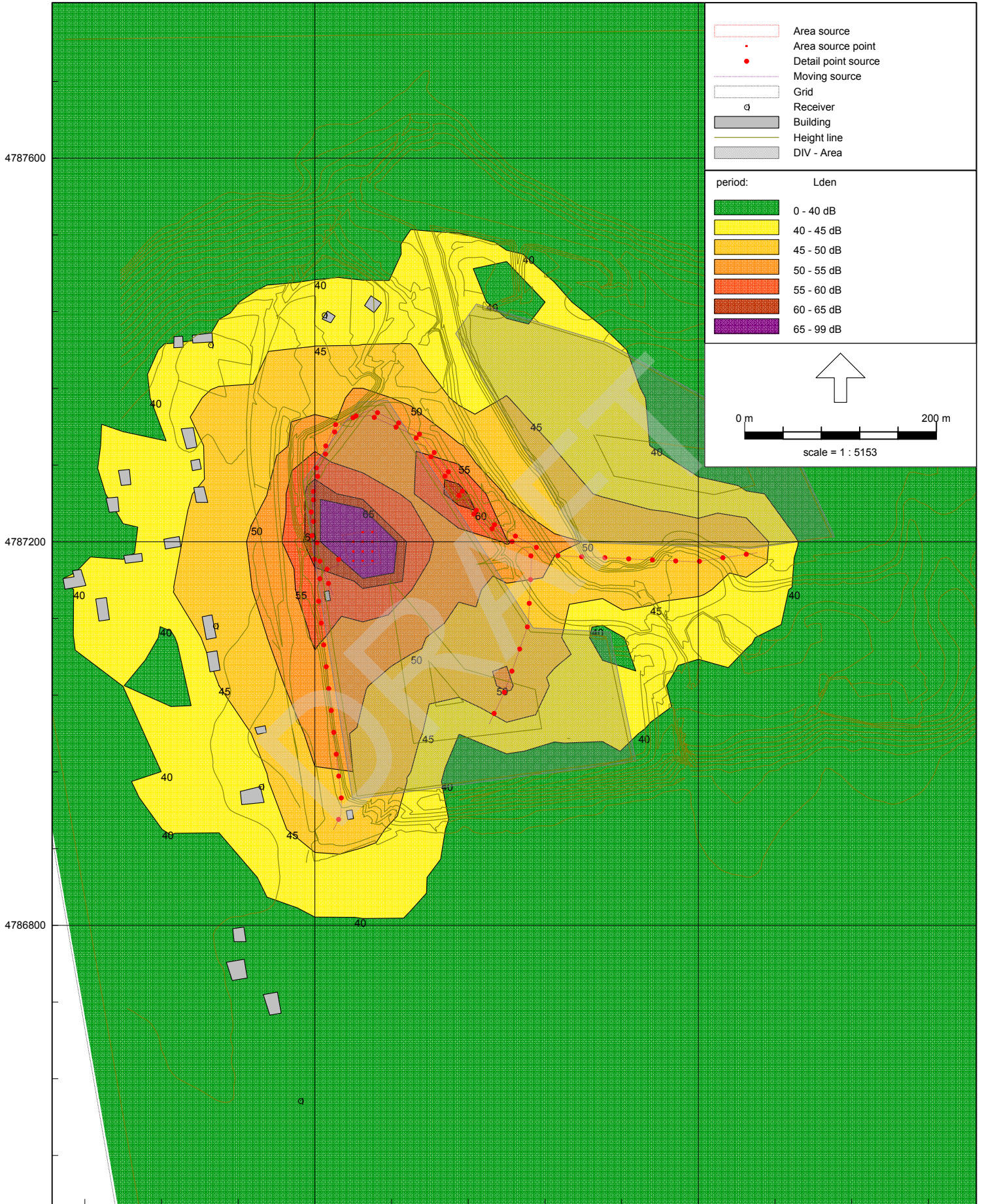
Figure 4-Exist Noise Contour (Current)

29 Mar 2016, 14:27











# BURNSIDE

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## Appendix A

### Off-Site Road Traffic AADT (Water Street South)

DRAFT

Road	2012 AADT*	2015 AADT	% Trucks	% Heavys	% Cars
Perth Road 123 (Weekday)	2125	2189	2	12	86
Landfill Site Driveway Access (Weekday)		180**	0	9	91
Landfill Site Driveway Access (Saturday)		250***	8	0	92

\*Annual average daily traffic, obtained from Perth County

\*\*Obtained by multiplying a.m. OR p.m. peak hour (whichever is higher) volumes by 10

\*\*\*Obtained by multiplying a.m. peak hour volumes by 5

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# BURNSIDE

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## Appendix B

### STAMSON Noise Model Output

POR\_01  
POR\_02  
POR\_03  
POR\_04  
POR\_05  
POR\_06

DRAFT

Filename: Test.te Time Period: Day/Night 16/8 hours  
 Description: POR1 OLA Water Street

Road data, segment # 1: Water St (day/night)

-----  
 Car traffic volume : 3744/416 veh/TimePeriod \*  
 Medium truck volume : 87/10 veh/TimePeriod \*  
 Heavy truck volume : 522/58 veh/TimePeriod \*  
 Posted speed limit : 80 km/h  
 Road gradient : 0 %  
 Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 4379  
 Percentage of Annual Growth : 1.00  
 Number of Years of Growth : 10.00  
 Medium Truck % of Total Volume : 2.00  
 Heavy Truck % of Total Volume : 12.00  
 Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 1: Water St (day/night)

-----  
 Angle1 Angle2 : -90.00 deg 90.00 deg  
 Wood depth : 0 (No woods.)  
 No of house rows : 0 / 0  
 Surface : 1 (Absorptive ground surface)  
 Receiver source distance : 29.81 / 29.81 m  
 Receiver height : 1.50 / 1.50 m  
 Topography : 1 (Flat/gentle slope; no barrier)  
 Reference angle : 0.00

♀  
 Results segment # 1: Water St (day)

-----  
 Source height = 1.86 m

ROAD (0.00 + 62.88 + 0.00) = 62.88 dBA  

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	w.Adj	H.Adj	B.Adj	SubLeq
-90	90	0.65	69.24	0.00	-4.92	-1.44	0.00	0.00	0.00	62.88

Segment Leq : 62.88 dBA

Total Leq All Segments: 62.88 dBA

♀  
 Results segment # 1: Water St (night)

-----  
 Source height = 1.86 m

ROAD (0.00 + 56.36 + 0.00) = 56.36 dBA  

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	w.Adj	H.Adj	B.Adj	SubLeq
-90	90	0.65	62.72	0.00	-4.92	-1.44	0.00	0.00	0.00	56.36



POR1\_OLA

Segment Leq : 56.36 dBA

Total Leq All Segments: 56.36 dBA

♀

TOTAL Leq FROM ALL SOURCES (DAY): 62.88  
(NIGHT): 56.36

♀  
♂

DRAFT

Filename: por1\_pow.te Time Period: Day/Night 16/8 hours  
 Description: POR1 POW Water Street

Road data, segment # 1: Water St (day/night)

-----  
 Car traffic volume : 3744/416 veh/TimePeriod \*  
 Medium truck volume : 87/10 veh/TimePeriod \*  
 Heavy truck volume : 522/58 veh/TimePeriod \*  
 Posted speed limit : 80 km/h  
 Road gradient : 0 %  
 Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 4379  
 Percentage of Annual Growth : 1.00  
 Number of Years of Growth : 10.00  
 Medium Truck % of Total Volume : 2.00  
 Heavy Truck % of Total Volume : 12.00  
 Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 1: Water St (day/night)

-----  
 Angle1 Angle2 : -90.00 deg 90.00 deg  
 Wood depth : 0 (No woods.)  
 No of house rows : 0 / 0  
 Surface : 1 (Absorptive ground surface)  
 Receiver source distance : 26.81 / 26.81 m  
 Receiver height : 4.50 / 4.50 m  
 Topography : 1 (Flat/gentle slope; no barrier)  
 Reference angle : 0.00

♀  
 Results segment # 1: Water St (day)

-----  
 Source height = 1.86 m

ROAD (0.00 + 64.03 + 0.00) = 64.03 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	w.Adj	H.Adj	B.Adj	SubLeq
-90	90	0.56	69.24	0.00	-3.93	-1.28	0.00	0.00	0.00	64.03

Segment Leq : 64.03 dBA

Total Leq All Segments: 64.03 dBA

♀  
 Results segment # 1: Water St (night)

-----  
 Source height = 1.86 m

ROAD (0.00 + 57.50 + 0.00) = 57.50 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	w.Adj	H.Adj	B.Adj	SubLeq
-90	90	0.56	62.72	0.00	-3.93	-1.28	0.00	0.00	0.00	57.50

POR1\_POW

Segment Leq : 57.50 dBA

Total Leq All Segments: 57.50 dBA

♀

TOTAL Leq FROM ALL SOURCES (DAY): 64.03  
(NIGHT): 57.50

♀  
♂

DRAFT

Filename: por2\_ola.te Time Period: Day/Night 16/8 hours  
 Description: POR2 OLA Water Street

Road data, segment # 1: Water St (day/night)

-----  
 Car traffic volume : 3744/416 veh/TimePeriod \*  
 Medium truck volume : 87/10 veh/TimePeriod \*  
 Heavy truck volume : 522/58 veh/TimePeriod \*  
 Posted speed limit : 80 km/h  
 Road gradient : 0 %  
 Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 4379  
 Percentage of Annual Growth : 1.00  
 Number of Years of Growth : 10.00  
 Medium Truck % of Total Volume : 2.00  
 Heavy Truck % of Total Volume : 12.00  
 Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 1: Water St (day/night)

-----  
 Angle1 Angle2 : -65.00 deg 61.00 deg  
 Wood depth : 0 (No woods.)  
 No of house rows : 0 / 0  
 Surface : 1 (Absorptive ground surface)  
 Receiver source distance : 68.02 / 68.02 m  
 Receiver height : 1.50 / 1.50 m  
 Topography : 1 (Flat/gentle slope; no barrier)  
 Reference angle : 0.00

♀  
 Results segment # 1: Water St (day)

-----  
 Source height = 1.86 m

ROAD (0.00 + 56.25 + 0.00) = 56.25 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	w.Adj	H.Adj	B.Adj	SubLeq
-65	61	0.65	69.24	0.00	-10.83	-2.17	0.00	0.00	0.00	56.25

Segment Leq : 56.25 dBA

Total Leq All Segments: 56.25 dBA

♀  
 Results segment # 1: Water St (night)

-----  
 Source height = 1.86 m

ROAD (0.00 + 49.72 + 0.00) = 49.72 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	w.Adj	H.Adj	B.Adj	SubLeq
-65	61	0.65	62.72	0.00	-10.83	-2.17	0.00	0.00	0.00	49.72

Segment Leq : 49.72 dBA

Total Leq All Segments: 49.72 dBA

♀

TOTAL Leq FROM ALL SOURCES (DAY): 56.25  
(NIGHT): 49.72

♀  
♂

DRAFT

Filename: por2\_pow.te Time Period: Day/Night 16/8 hours  
 Description: POR2 POW Water Street

Road data, segment # 1: Water St (day/night)

-----  
 Car traffic volume : 3744/416 veh/TimePeriod \*  
 Medium truck volume : 87/10 veh/TimePeriod \*  
 Heavy truck volume : 522/58 veh/TimePeriod \*  
 Posted speed limit : 80 km/h  
 Road gradient : 0 %  
 Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 4379  
 Percentage of Annual Growth : 1.00  
 Number of Years of Growth : 10.00  
 Medium Truck % of Total Volume : 2.00  
 Heavy Truck % of Total Volume : 12.00  
 Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 1: Water St (day/night)

-----  
 Angle1 Angle2 : -69.00 deg 60.00 deg  
 Wood depth : 0 (No woods.)  
 No of house rows : 0 / 0  
 Surface : 1 (Absorptive ground surface)  
 Receiver source distance : 45.17 / 45.17 m  
 Receiver height : 4.50 / 4.50 m  
 Topography : 1 (Flat/gentle slope; no barrier)  
 Reference angle : 0.00

♀  
 Results segment # 1: Water St (day)

-----  
 Source height = 1.86 m

ROAD (0.00 + 59.76 + 0.00) = 59.76 dBA  

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	w.Adj	H.Adj	B.Adj	SubLeq
-69	60	0.56	69.24	0.00	-7.46	-2.02	0.00	0.00	0.00	59.76

Segment Leq : 59.76 dBA

Total Leq All Segments: 59.76 dBA

♀  
 Results segment # 1: Water St (night)

-----  
 Source height = 1.86 m

ROAD (0.00 + 53.23 + 0.00) = 53.23 dBA  

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	w.Adj	H.Adj	B.Adj	SubLeq
-69	60	0.56	62.72	0.00	-7.46	-2.02	0.00	0.00	0.00	53.23

POR2\_POW

Segment Leq : 53.23 dBA

Total Leq All Segments: 53.23 dBA

♀

TOTAL Leq FROM ALL SOURCES (DAY): 59.76  
(NIGHT): 53.23

♀  
♂

DRAFT

Filename: por3\_ola.te                      Time Period: Day/Night 16/8 hours  
 Description: POR3 OLA Water Street

Road data, segment # 1: Water St (day/night)

-----  
 Car traffic volume : 3744/416    veh/TimePeriod    \*  
 Medium truck volume : 87/10    veh/TimePeriod    \*  
 Heavy truck volume : 522/58    veh/TimePeriod    \*  
 Posted speed limit : 80 km/h  
 Road gradient : 0 %  
 Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 4379  
 Percentage of Annual Growth : 1.00  
 Number of Years of Growth : 10.00  
 Medium Truck % of Total Volume : 2.00  
 Heavy Truck % of Total Volume : 12.00  
 Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 1: Water St (day/night)

-----  
 Angle1    Angle2                      : -77.00 deg    67.00 deg  
 Wood depth : 0    (No woods.)  
 No of house rows : 0 / 0  
 Surface : 1    (Absorptive ground surface)  
 Receiver source distance : 72.79 / 72.79 m  
 Receiver height : 1.50 / 1.50 m  
 Topography : 1    (Flat/gentle slope; no barrier)  
 Reference angle : 0.00

♀  
 Results segment # 1: Water St (day)

-----  
 Source height = 1.86 m

ROAD (0.00 + 56.12 + 0.00) = 56.12 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	w.Adj	H.Adj	B.Adj	SubLeq
-77	67	0.65	69.24	0.00	-11.31	-1.81	0.00	0.00	0.00	56.12

-----

Segment Leq : 56.12 dBA

Total Leq All Segments: 56.12 dBA

♀  
 Results segment # 1: Water St (night)

-----  
 Source height = 1.86 m

ROAD (0.00 + 49.59 + 0.00) = 49.59 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	w.Adj	H.Adj	B.Adj	SubLeq
-77	67	0.65	62.72	0.00	-11.31	-1.81	0.00	0.00	0.00	49.59

-----



Segment Leq : 49.59 dBA

Total Leq All Segments: 49.59 dBA

♀

TOTAL Leq FROM ALL SOURCES (DAY): 56.12  
(NIGHT): 49.59

♀  
♂

DRAFT

Filename: por3\_pow.te Time Period: Day/Night 16/8 hours  
 Description: POR3 POW Water Street

Road data, segment # 1: Water St (day/night)

-----  
 Car traffic volume : 3744/416 veh/TimePeriod \*  
 Medium truck volume : 87/10 veh/TimePeriod \*  
 Heavy truck volume : 522/58 veh/TimePeriod \*  
 Posted speed limit : 80 km/h  
 Road gradient : 0 %  
 Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 4379  
 Percentage of Annual Growth : 1.00  
 Number of Years of Growth : 10.00  
 Medium Truck % of Total Volume : 2.00  
 Heavy Truck % of Total Volume : 12.00  
 Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 1: Water St (day/night)

-----  
 Angle1 Angle2 : -70.00 deg 65.00 deg  
 Wood depth : 0 (No woods.)  
 No of house rows : 0 / 0  
 Surface : 1 (Absorptive ground surface)  
 Receiver source distance : 59.24 / 59.24 m  
 Receiver height : 4.50 / 4.50 m  
 Topography : 1 (Flat/gentle slope; no barrier)  
 Reference angle : 0.00

♀  
 Results segment # 1: Water St (day)

-----  
 Source height = 1.86 m

ROAD (0.00 + 58.06 + 0.00) = 58.06 dBA  

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-70	65	0.56	69.24	0.00	-9.30	-1.88	0.00	0.00	0.00	58.06

Segment Leq : 58.06 dBA

Total Leq All Segments: 58.06 dBA

♀  
 Results segment # 1: Water St (night)

-----  
 Source height = 1.86 m

ROAD (0.00 + 51.54 + 0.00) = 51.54 dBA  

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	W.Adj	H.Adj	B.Adj	SubLeq
-70	65	0.56	62.72	0.00	-9.30	-1.88	0.00	0.00	0.00	51.54

POR3\_POW

Segment Leq : 51.54 dBA

Total Leq All Segments: 51.54 dBA

♀

TOTAL Leq FROM ALL SOURCES (DAY): 58.06  
(NIGHT): 51.54

♀  
♂

DRAFT

Filename: por4\_ola.te Time Period: Day/Night 16/8 hours  
 Description: POR4 OLA Water Street

Road data, segment # 1: Water St (day/night)

-----  
 Car traffic volume : 3744/416 veh/TimePeriod \*  
 Medium truck volume : 87/10 veh/TimePeriod \*  
 Heavy truck volume : 522/58 veh/TimePeriod \*  
 Posted speed limit : 80 km/h  
 Road gradient : 0 %  
 Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 4379  
 Percentage of Annual Growth : 1.00  
 Number of Years of Growth : 10.00  
 Medium Truck % of Total Volume : 2.00  
 Heavy Truck % of Total Volume : 12.00  
 Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 1: Water St (day/night)

-----  
 Angle1 Angle2 : -60.00 deg 90.00 deg  
 Wood depth : 0 (No woods.)  
 No of house rows : 0 / 0  
 Surface : 1 (Absorptive ground surface)  
 Receiver source distance : 46.95 / 46.95 m  
 Receiver height : 1.50 / 1.50 m  
 Topography : 1 (Flat/gentle slope; no barrier)  
 Reference angle : 0.00

♀  
 Results segment # 1: Water St (day)

-----  
 Source height = 1.86 m

ROAD (0.00 + 59.22 + 0.00) = 59.22 dBA  

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	w.Adj	H.Adj	B.Adj	SubLeq
-60	90	0.65	69.24	0.00	-8.17	-1.85	0.00	0.00	0.00	59.22

Segment Leq : 59.22 dBA

Total Leq All Segments: 59.22 dBA

♀  
 Results segment # 1: Water St (night)

-----  
 Source height = 1.86 m

ROAD (0.00 + 52.69 + 0.00) = 52.69 dBA  

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	w.Adj	H.Adj	B.Adj	SubLeq
-60	90	0.65	62.72	0.00	-8.17	-1.85	0.00	0.00	0.00	52.69

Segment Leq : 52.69 dBA

Total Leq All Segments: 52.69 dBA

♀

TOTAL Leq FROM ALL SOURCES (DAY): 59.22  
(NIGHT): 52.69

♀  
♂

DRAFT

Filename: por4\_pow.te                      Time Period: Day/Night 16/8 hours  
 Description: POR4 POW Water Street

Road data, segment # 1: Water St (day/night)

-----  
 Car traffic volume : 3744/416    veh/TimePeriod    \*  
 Medium truck volume : 87/10    veh/TimePeriod    \*  
 Heavy truck volume : 522/58    veh/TimePeriod    \*  
 Posted speed limit : 80 km/h  
 Road gradient : 0 %  
 Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 4379  
 Percentage of Annual Growth : 1.00  
 Number of Years of Growth : 10.00  
 Medium Truck % of Total Volume : 2.00  
 Heavy Truck % of Total Volume : 12.00  
 Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 1: Water St (day/night)

-----  
 Angle1    Angle2                      : -90.00 deg    90.00 deg  
 Wood depth : 0    (No woods.)  
 No of house rows : 0 / 0  
 Surface : 1    (Absorptive ground surface)  
 Receiver source distance : 31.61 / 31.61 m  
 Receiver height : 4.50 / 4.50 m  
 Topography : 1    (Flat/gentle slope; no barrier)  
 Reference angle : 0.00

♀  
 Results segment # 1: Water St (day)

-----  
 Source height = 1.86 m

ROAD (0.00 + 62.91 + 0.00) = 62.91 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	w.Adj	H.Adj	B.Adj	SubLeq
-90	90	0.56	69.24	0.00	-5.05	-1.28	0.00	0.00	0.00	62.91

-----

Segment Leq : 62.91 dBA

Total Leq All Segments: 62.91 dBA

♀  
 Results segment # 1: Water St (night)

-----  
 Source height = 1.86 m

ROAD (0.00 + 56.39 + 0.00) = 56.39 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	w.Adj	H.Adj	B.Adj	SubLeq
-90	90	0.56	62.72	0.00	-5.05	-1.28	0.00	0.00	0.00	56.39

-----

POR4\_POW

Segment Leq : 56.39 dBA

Total Leq All Segments: 56.39 dBA

♀

TOTAL Leq FROM ALL SOURCES (DAY): 62.91  
(NIGHT): 56.39

♀  
♂

DRAFT

Filename: por5\_ola.te Time Period: Day/Night 16/8 hours  
 Description: POR5 OLA Water Street

Road data, segment # 1: Water St (day/night)

-----  
 Car traffic volume : 3744/416 veh/TimePeriod \*  
 Medium truck volume : 87/10 veh/TimePeriod \*  
 Heavy truck volume : 522/58 veh/TimePeriod \*  
 Posted speed limit : 80 km/h  
 Road gradient : 0 %  
 Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 4379  
 Percentage of Annual Growth : 1.00  
 Number of Years of Growth : 10.00  
 Medium Truck % of Total Volume : 2.00  
 Heavy Truck % of Total Volume : 12.00  
 Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 1: Water St (day/night)

-----  
 Angle1 Angle2 : -85.00 deg 90.00 deg  
 Wood depth : 0 (No woods.)  
 No of house rows : 0 / 0  
 Surface : 1 (Absorptive ground surface)  
 Receiver source distance : 55.00 / 55.00 m  
 Receiver height : 1.50 / 1.50 m  
 Topography : 1 (Flat/gentle slope; no barrier)  
 Reference angle : 0.00

♀  
 Results segment # 1: Water St (day)

-----  
 Source height = 1.86 m

ROAD (0.00 + 58.48 + 0.00) = 58.48 dBA  

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	w.Adj	H.Adj	B.Adj	SubLeq
-85	90	0.65	69.24	0.00	-9.31	-1.46	0.00	0.00	0.00	58.48

Segment Leq : 58.48 dBA

Total Leq All Segments: 58.48 dBA

♀  
 Results segment # 1: Water St (night)

-----  
 Source height = 1.86 m

ROAD (0.00 + 51.95 + 0.00) = 51.95 dBA  

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	w.Adj	H.Adj	B.Adj	SubLeq
-85	90	0.65	62.72	0.00	-9.31	-1.46	0.00	0.00	0.00	51.95



Segment Leq : 51.95 dBA

Total Leq All Segments: 51.95 dBA

♀

TOTAL Leq FROM ALL SOURCES (DAY): 58.48  
(NIGHT): 51.95

♀  
♂

DRAFT

Filename: por5\_pow.te Time Period: Day/Night 16/8 hours  
 Description: POR5 POW Water Street

Road data, segment # 1: Water St (day/night)

-----  
 Car traffic volume : 3744/416 veh/TimePeriod \*  
 Medium truck volume : 87/10 veh/TimePeriod \*  
 Heavy truck volume : 522/58 veh/TimePeriod \*  
 Posted speed limit : 80 km/h  
 Road gradient : 0 %  
 Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 4379  
 Percentage of Annual Growth : 1.00  
 Number of Years of Growth : 10.00  
 Medium Truck % of Total Volume : 2.00  
 Heavy Truck % of Total Volume : 12.00  
 Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 1: Water St (day/night)

-----  
 Angle1 Angle2 : -90.00 deg 90.00 deg  
 Wood depth : 0 (No woods.)  
 No of house rows : 0 / 0  
 Surface : 1 (Absorptive ground surface)  
 Receiver source distance : 36.96 / 36.96 m  
 Receiver height : 4.50 / 4.50 m  
 Topography : 1 (Flat/gentle slope; no barrier)  
 Reference angle : 0.00

♀  
 Results segment # 1: Water St (day)

-----  
 Source height = 1.86 m

ROAD (0.00 + 61.85 + 0.00) = 61.85 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	w.Adj	H.Adj	B.Adj	SubLeq
-90	90	0.56	69.24	0.00	-6.11	-1.28	0.00	0.00	0.00	61.85

Segment Leq : 61.85 dBA

Total Leq All Segments: 61.85 dBA

♀  
 Results segment # 1: Water St (night)

-----  
 Source height = 1.86 m

ROAD (0.00 + 55.33 + 0.00) = 55.33 dBA

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	w.Adj	H.Adj	B.Adj	SubLeq
-90	90	0.56	62.72	0.00	-6.11	-1.28	0.00	0.00	0.00	55.33

POR5\_POW

Segment Leq : 55.33 dBA

Total Leq All Segments: 55.33 dBA

♀

TOTAL Leq FROM ALL SOURCES (DAY): 61.85  
(NIGHT): 55.33

♀  
♂

DRAFT

Filename: por6\_ola.te Time Period: Day/Night 16/8 hours  
 Description: POR6 OLA Water Street

Road data, segment # 1: Water St (day/night)

-----  
 Car traffic volume : 3744/416 veh/TimePeriod \*  
 Medium truck volume : 87/10 veh/TimePeriod \*  
 Heavy truck volume : 522/58 veh/TimePeriod \*  
 Posted speed limit : 80 km/h  
 Road gradient : 0 %  
 Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 4379  
 Percentage of Annual Growth : 1.00  
 Number of Years of Growth : 10.00  
 Medium Truck % of Total Volume : 2.00  
 Heavy Truck % of Total Volume : 12.00  
 Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 1: Water St (day/night)

-----  
 Angle1 Angle2 : -85.00 deg 90.00 deg  
 Wood depth : 0 (No woods.)  
 No of house rows : 0 / 0  
 Surface : 1 (Absorptive ground surface)  
 Receiver source distance : 43.57 / 43.57 m  
 Receiver height : 1.50 / 1.50 m  
 Topography : 1 (Flat/gentle slope; no barrier)  
 Reference angle : 0.00

♀  
 Results segment # 1: Water St (day)

-----  
 Source height = 1.86 m

ROAD (0.00 + 60.15 + 0.00) = 60.15 dBA  

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	w.Adj	H.Adj	B.Adj	SubLeq
-85	90	0.65	69.24	0.00	-7.64	-1.46	0.00	0.00	0.00	60.15

Segment Leq : 60.15 dBA

Total Leq All Segments: 60.15 dBA

♀  
 Results segment # 1: Water St (night)

-----  
 Source height = 1.86 m

ROAD (0.00 + 53.62 + 0.00) = 53.62 dBA  

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	w.Adj	H.Adj	B.Adj	SubLeq
-85	90	0.65	62.72	0.00	-7.64	-1.46	0.00	0.00	0.00	53.62

Segment Leq : 53.62 dBA

Total Leq All Segments: 53.62 dBA

♀

TOTAL Leq FROM ALL SOURCES (DAY): 60.15  
(NIGHT): 53.62

♀  
♂

DRAFT

Filename: por6\_pow.te Time Period: Day/Night 16/8 hours  
 Description: POR6 POW Water Street

Road data, segment # 1: Water St (day/night)

-----  
 Car traffic volume : 3744/416 veh/TimePeriod \*  
 Medium truck volume : 87/10 veh/TimePeriod \*  
 Heavy truck volume : 522/58 veh/TimePeriod \*  
 Posted speed limit : 80 km/h  
 Road gradient : 0 %  
 Road pavement : 1 (Typical asphalt or concrete)

\* Refers to calculated road volumes based on the following input:

24 hr Traffic Volume (AADT or SADT): 4379  
 Percentage of Annual Growth : 1.00  
 Number of Years of Growth : 10.00  
 Medium Truck % of Total Volume : 2.00  
 Heavy Truck % of Total Volume : 12.00  
 Day (16 hrs) % of Total Volume : 90.00

Data for Segment # 1: Water St (day/night)

-----  
 Angle1 Angle2 : -90.00 deg 90.00 deg  
 Wood depth : 0 (No woods.)  
 No of house rows : 0 / 0  
 Surface : 1 (Absorptive ground surface)  
 Receiver source distance : 32.27 / 32.27 m  
 Receiver height : 4.50 / 4.50 m  
 Topography : 1 (Flat/gentle slope; no barrier)  
 Reference angle : 0.00

♀  
 Results segment # 1: Water St (day)

-----  
 Source height = 1.86 m

ROAD (0.00 + 62.77 + 0.00) = 62.77 dBA  

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	w.Adj	H.Adj	B.Adj	SubLeq
-90	90	0.56	69.24	0.00	-5.19	-1.28	0.00	0.00	0.00	62.77

Segment Leq : 62.77 dBA

Total Leq All Segments: 62.77 dBA

♀  
 Results segment # 1: Water St (night)

-----  
 Source height = 1.86 m

ROAD (0.00 + 56.25 + 0.00) = 56.25 dBA  

Angle1	Angle2	Alpha	RefLeq	P.Adj	D.Adj	F.Adj	w.Adj	H.Adj	B.Adj	SubLeq
-90	90	0.56	62.72	0.00	-5.19	-1.28	0.00	0.00	0.00	56.25

POR6\_POW

Segment Leq : 56.25 dBA

Total Leq All Segments: 56.25 dBA

♀

TOTAL Leq FROM ALL SOURCES (DAY): 62.77  
(NIGHT): 56.25

♀  
♂

DRAFT



# BURNSIDE

[ THE DIFFERENCE IS OUR PEOPLE ]

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## Appendix C Source Measurements and Sound Power Calculations

Table C01 - OnSite Trk  
Table C02 - CMPTR

DRAFT



Name	ID	Type	Octave Spectrum (dB)										
			Weight.	31.5	63	125	250	500	1000	2000	4000	8000 A	lin
Delivery Trucks	TThigh	Lw		105.1	112	115.3	113.9	109.9	105.4	98.2	90.2	115.1	119.6
Delivery Truck medium speed	TTmed	Lw		95.1	102	105.3	103.9	99.9	95.4	88.2	80.2	105.1	109.6
Delivery Truck at idle	TTidle	Lw		97.7	97.4	94.6	95.2	95.9	90.2	80.6	71.3	98.8	103.5
			Octave Spectrum (dBA)										
a-weight adjustment			-39.4	-26.2	-16.1	-8.6	-3.2	1E-12	1.2	1	-1.1		
Delivery Trucks	TThigh	Lw		78.9	95.9	106.7	110.7	109.9	106.6	99.2	89.1	115.1	
Delivery Truck medium speed	TTmed	Lw		68.9	85.9	96.7	100.7	99.9	96.6	89.2	79.1	105.1	
Delivery Truck at idle	TTidle	Lw		71.5	81.3	86	92	95.9	91.4	81.6	70.2	98.8	

DRAFT

SOURCE Des: Compactor 1986 CAT 816D

Tonal Indicator:

SOURCE TYP: Spherical Sphere 1/ 2  
 Enabled 1 1 1 1

Lw Technique: Spherical, Parallelepiped, or Area	Point 1	Point 2	Point 3	Point 4	# of Points	Average Lpf	LwfA (from Lwf)	Octave Sound Power
	Radius (m)	Radius (m)	Radius (m)	Radius (m)		L'p		
(Hz)	15.000	15.000	15.000	15.000	315.0000			
	Lpfi in dB	Lpfi in dB	Lpfi in dB	Lpfi in dB		(dB)	(dBA)	(dBA)
FileID	001	002	003					
Comment								
12.5	70.7	73.3	60.4		3	70.53	102.0	104.16
16	70.5	70.1	57.8		3	68.63	100.1	
20	63.3	67.3	56.2		3	64.24	45.2	
25	60.9	65.5	55.4		3	62.29	49.1	59.43
32	61.1	65.4	64.3		3	63.93	56.0	
40	59.0	61.2	55.5		3	59.14	56.0	
50	58.1	63.3	60.8		3	61.19	62.5	78.16
63	57.4	62.1	59.2		3	59.99	65.3	
80	69.7	67.8	68.7		3	68.81	77.8	
100	68.4	76.5	81.5		3	78.04	90.4	95.46
125	68.1	81.6	72.7		3	77.54	92.9	
160	64.0	71.8	66.4		3	68.65	86.7	
200	61.3	69.9	62.8		3	66.40	87.0	94.06
250	58.6	71.3	66.9		3	68.02	90.9	
315	58.4	66.7	63.9		3	64.17	89.1	
400	62.0	66.5	62.5		3	64.18	90.9	98.58
500	63.9	68.4	66.2		3	66.55	94.9	
630	61.1	67.0	65.0		3	64.99	94.6	
800	66.7	67.2	66.4		3	66.79	97.5	104.22
1,000	69.9	70.9	64.2		3	69.13	100.6	
1,250	66.5	68.2	67.8		3	67.56	99.7	
1,600	64.8	68.0	64.6		3	66.10	98.6	101.25
2,000	63.1	65.1	62.7		3	63.77	96.5	
2,500	57.5	61.3	57.9		3	59.27	92.1	
3,150	56.3	60.4	59.0		3	58.91	91.6	95.74
4,000	57.1	59.4	59.7		3	58.85	91.3	
5,000	56.4	58.3	58.4		3	57.78	89.8	
6,300	50.8	54.0	53.0		3	52.80	84.2	86.36
8,000	48.8	51.1	50.8		3	50.35	80.8	
10,000	44.5	49.2	48.8		3	47.93	76.9	
12,500	39.8	45.9	43.8		3	43.81	71.0	71.97
16,000	34.1	41.7	39.9		3	39.55	64.5	
20,000	27.6	35.6	33.0		3	33.17	55.4	
Overall (dB)	79.5	85.3	83.4		3.0	88.1	109.2	
Overall (dBA)	77.3	79.5	75.2					



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## Appendix D

### Photographs of Noise Sources

Compactor (CMPTR)

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St. Marys Landfill Environmental Assessment – Noise Impact Assessment  
March 2016

**Photograph 1: Compactor (CMPTR)**





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## Appendix E

### Predictor Model Inputs

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St. Marys Landfill Environmental Assessment – Noise Impact Assessment  
March 2016

## **Appendix E**

### **Predictor Model Inputs**

Some of the results produced by the Predictor Noise propagation model are shown on the next page. The complete set of data is in the file on the CD. The file name is “032339.0000 St. Marys Noise Tables – Predictor.xls”.

Outputs start on row start on row 397.

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Receivers Limit of 88  
Group Item ID

Grp ID	Date	1st Kid	Kid Cnt	Name	Desc.	Shape	X	Y	Terrain L	HDef.
4	0 3/15/2016 15:00		-60	2 POR_04		Point	487144	4786945	324.61	Relative
5	0 3/15/2016 15:00		-66	2 POR_03		Point	487096.4	4787112	264.75	Relative
6	0 3/15/2016 15:00		-72	2 POR_02		Point	487091.4	4787405	324	Relative
7	0 3/17/2016 10:49		-78	2 POR_05		Point	487185	4786617	264.08	Relative
8	0 3/17/2016 10:49		-84	2 POR_06		Point	487326	4786203	0	Relative
67	0 3/15/2016 15:00		-249	2 POR_01		Point	487209.9	4787436	320.73	Relative

Area Source Limit of 20  
Group Item ID

Grp ID	Date	1st Kid	Kid Cnt	Name	Desc.	Shape	X1	Y1	Height	Rel.H
207	0 3/17/2016 9:19	#####		13 CMPTR	1986 C	Polygon	487259.5	4787100	2.8	2.8

Moving Source Limit of 20  
Group Item ID

Grp ID	Date	1st Kid	Kid Cnt	Name	Desc.	Shape	X1	Y1	Xn	Yn
251	0 3/15/2016 13:13		-2090	14 OnSiteTrk1	Entranc	Polyline	487215.7	4787129	487205.5	4786890
254	0 3/17/2016 7:42		-2508	4 OnSiteTrk2	Scale ti	Polyline	487217.5	4787125	487262.8	4787080
268	0 3/15/2016 10:31		-2385	30 OnSiteTrk3	Travelli	Polyline	487221.1	4787128	487858.6	4787109
272	0 3/15/2016 13:17		-2421	17 OnSiteTrk4	Travelli	Polyline	487222.7	4787126	487402.5	4786962

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## Appendix F

### Predictor Model Outputs

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St. Marys Landfill Environmental Assessment – Noise Impact Assessment  
March 2016

## **Appendix F**

### **Predictor Model Outputs**

Some of the results produced by the Predictor Noise propagation model are shown on the next page. The complete set of data is in the file on the CD. The file name is “032339.0000 St. Marys Noise Tables – Predictor.xls”.

Outputs start on row 1 and end on row 397.

DRAFT

Day Group / source	Limit 100 Sources, 88 PORs											
	Reducti		POR_04_A		POR_04_B		POR_03_A		POR_03_B		POR_02_A	
	[dB]	result	corr.	result	corr.	result	corr.	result	corr.	result	corr.	
CMPTR	0	45	45	47.9	47.9	44.1	44.1	48.5	48.5	38.3	38.3	
OnSiteTrk1	0	44.8	44.8	46.6	46.6	42.3	42.3	44.2	44.2	32.9	32.9	
OnSiteTrk2	0	28.4	28.4	30.5	30.5	30.2	30.2	32.3	32.3	22	22	
OnSiteTrk3	0	31.4	31.4	35.1	35.1	32.5	32.5	36.1	36.1	29.1	29.1	
OnSiteTrk4	0	28.9	28.9	32.3	32.3	29.6	29.6	33.1	33.1	25	25	
Total		48.1	48.1	50.6	50.6	46.7	46.7	50.2	50.2	40	40	

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